

The management of the Athens water resource system: Methodological issues

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Acknowledgments

A. Eftstratiadis, R. Mavrodemou, N. Mamassis, A Koukouvinos, I. Nalbantis

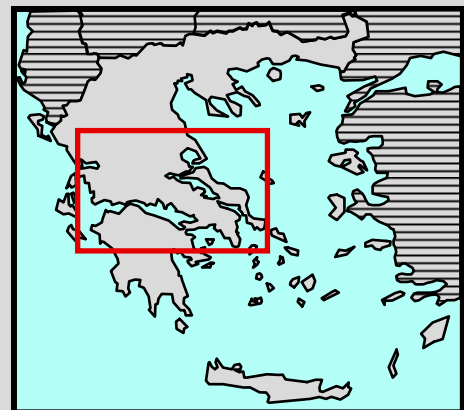
E. Rozos, M. Economou, G. Karavokyros

Not in photo: A. Christofides, S. Kozanis, O. Kitsou

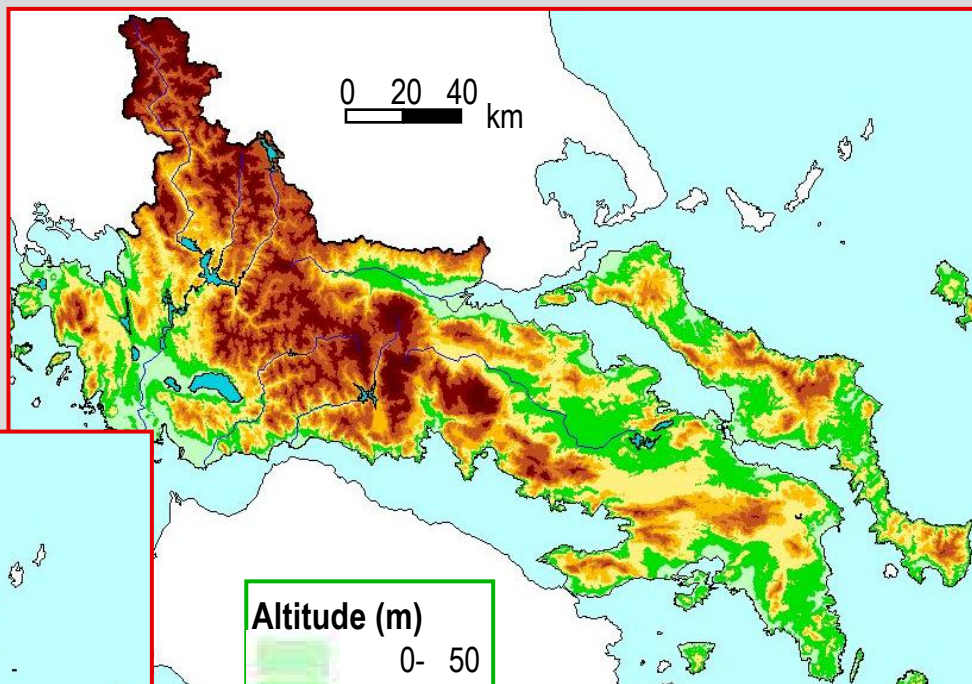
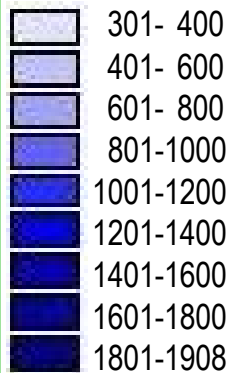


“Υσον, ὕσον Ζεῦ κατὰ τῆς ἀρούρης τῶν Ἀθηναίων

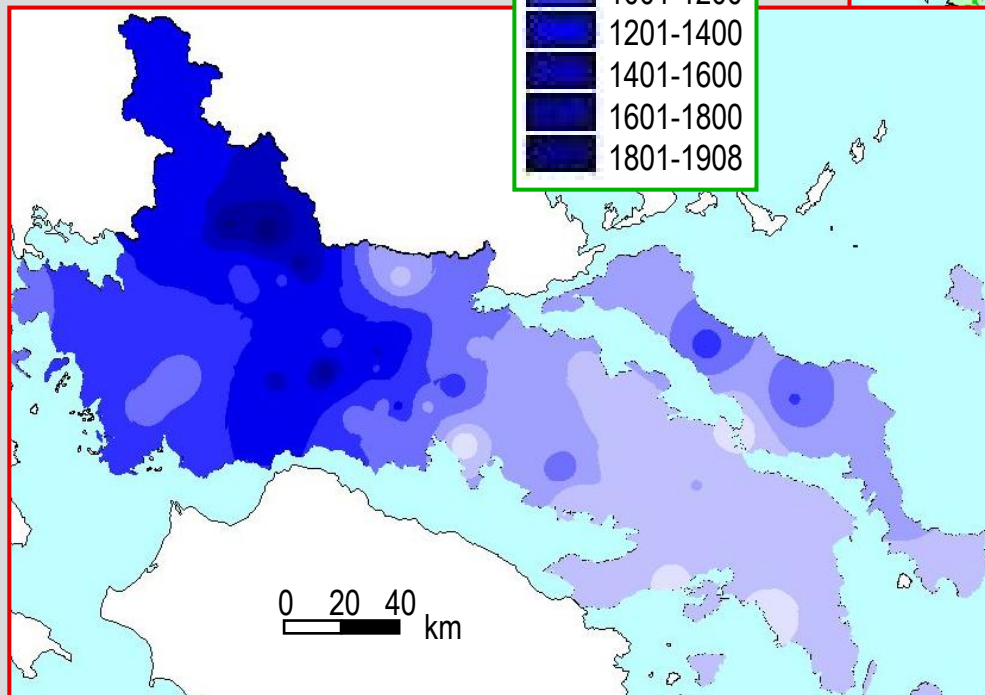
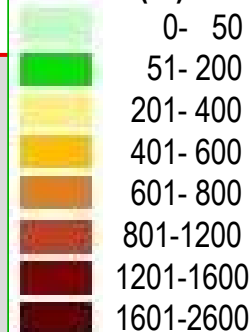
Do rain, do rain Zeus against the earth of Athenians (Ancient Greek prayer)



Mean annual rainfall (mm)



Altitude (m)



Parts of the presentation

1. The Athens water resource system

History – Components – Technical characteristics

2. Hydrologic issues

Diagnosis – Explanation – Operational synthesis

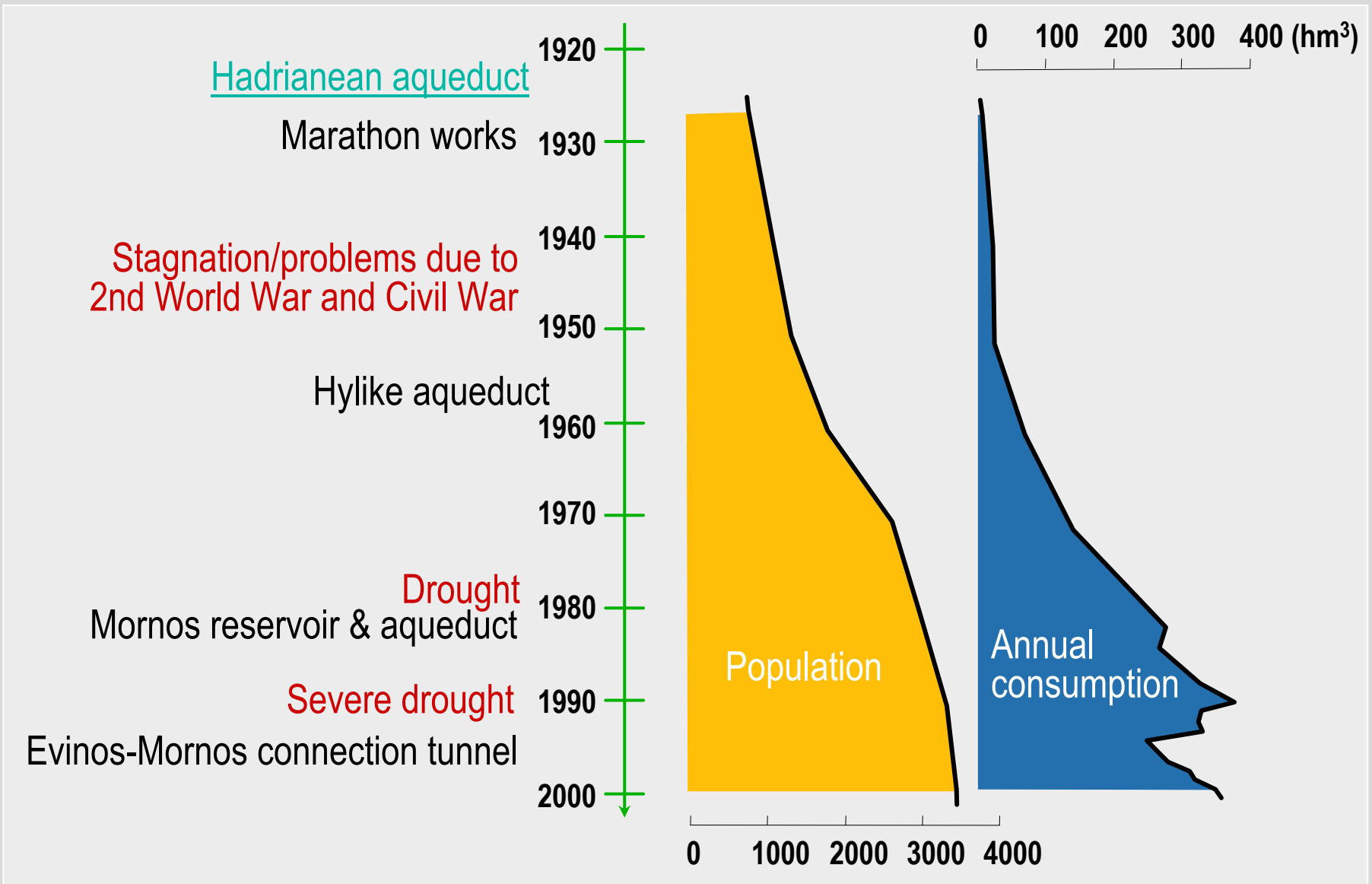
3. Hydrosystem operation issues

Parameterization – Simulation – Optimization

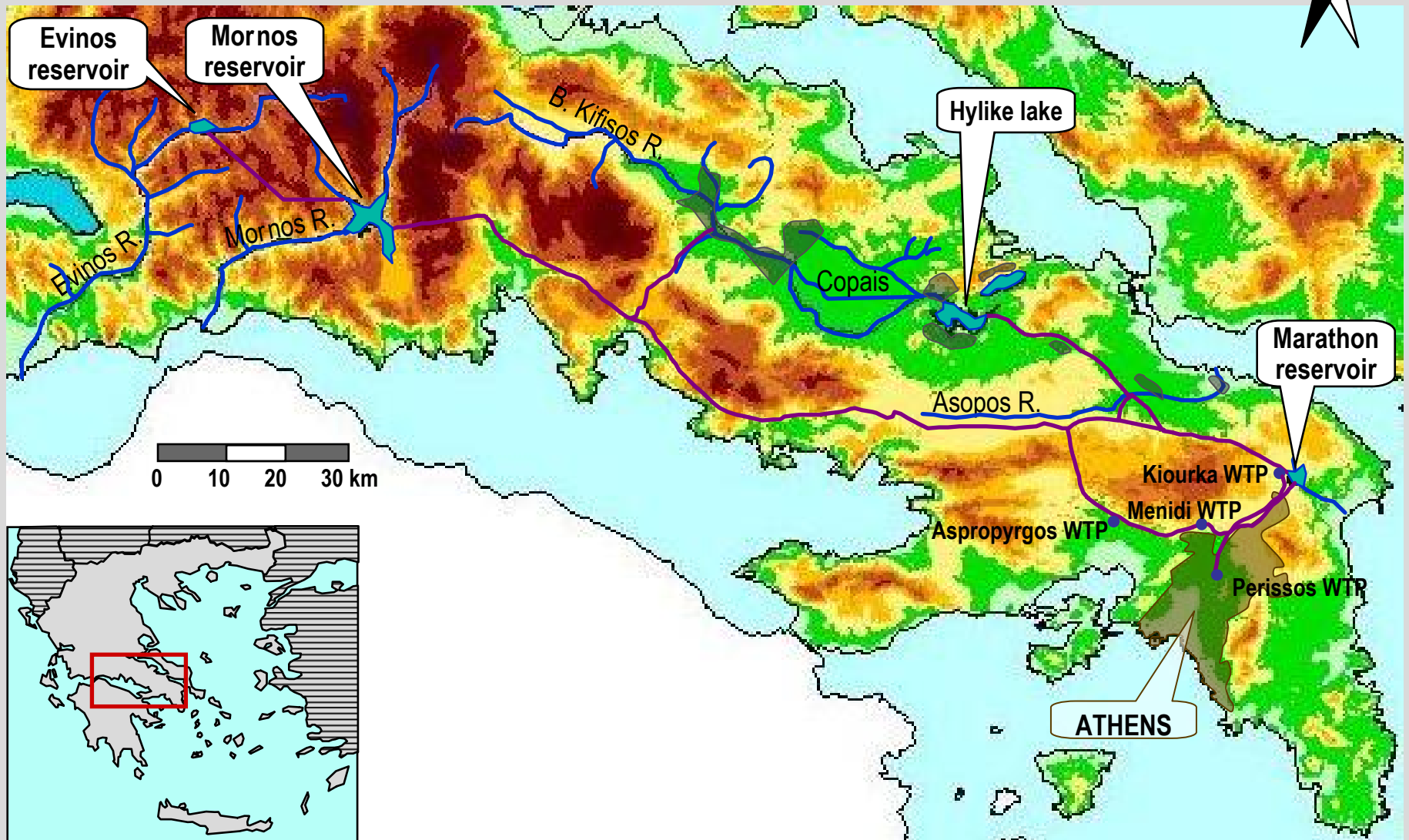
4. Decision support tool integration

Data acquisition – Software systems – Management plans






Evolution of water consumption – Milestones




The hydrosystem: Main components and evolution

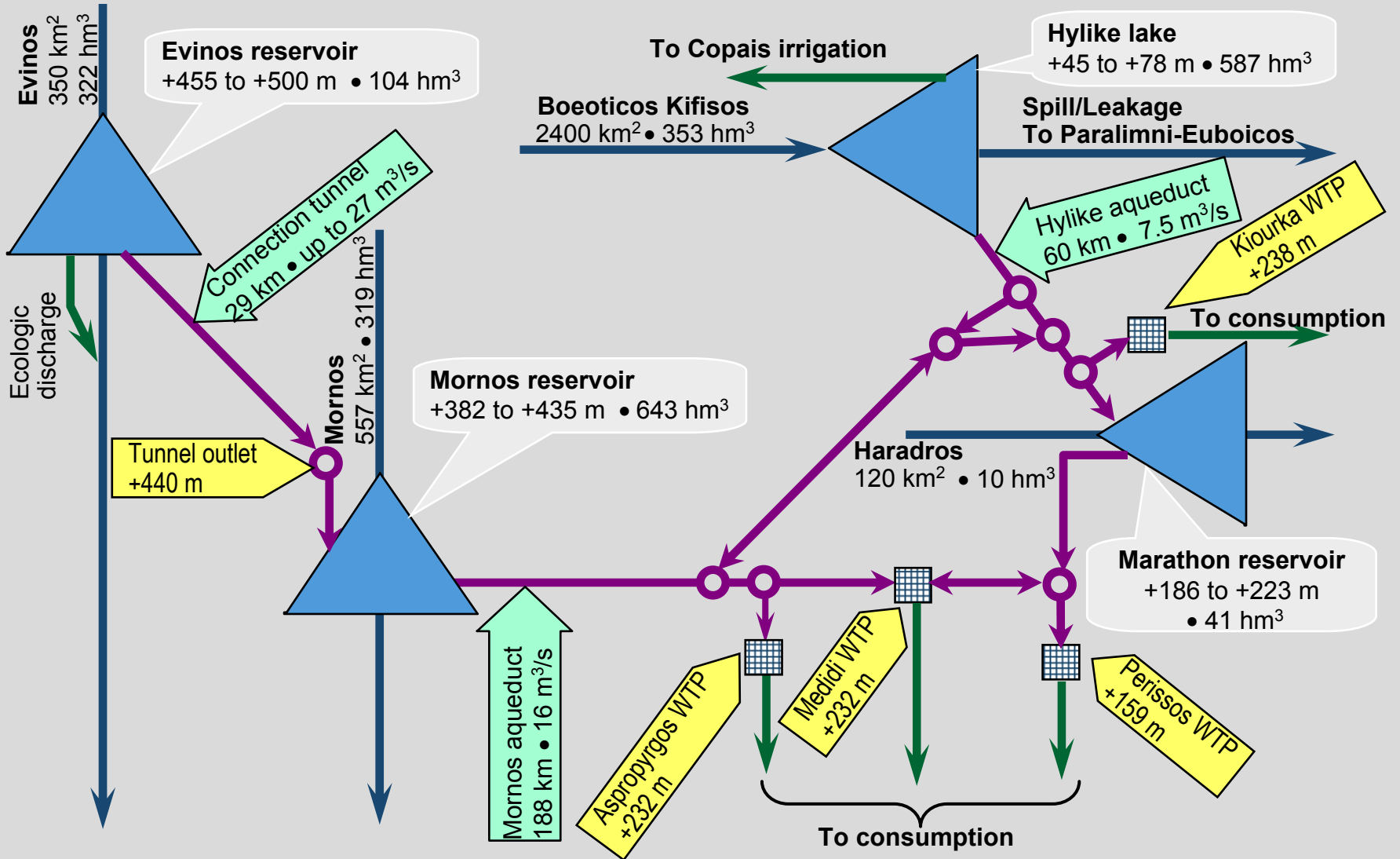


Classification of water resources

Basin	SURFACE WATER		GROUNDWATER
	Primary (Reservoirs)	Secondary (Reservoirs)	Backup (Boreholes)
Evinos 350 km ²	Evinos 322 hm ³ /y 		
Mornos 557 km ²	Mornos 319 hm ³ /y		
Boeotikos Kifisos – Yliki 2400 km ²		Yliki 353 hm ³ /y  	B. Kifisos, middle course 136 hm ³ /y Yliki region 85 hm ³ /y 
Haradros 120 km ²		Marathon 10 hm ³ /y	
North Parnetha			Viliza 26 hm ³ /y  Mavrosouvala 36 hm ³ /y

Area	Inflow	Pumping capacity 	High spill 	High leakage 	Pumping
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Hydrosystem: Current structure



+ Boreholes (with connecting pipes) + Pumping stations + Small hydroelectric power plants

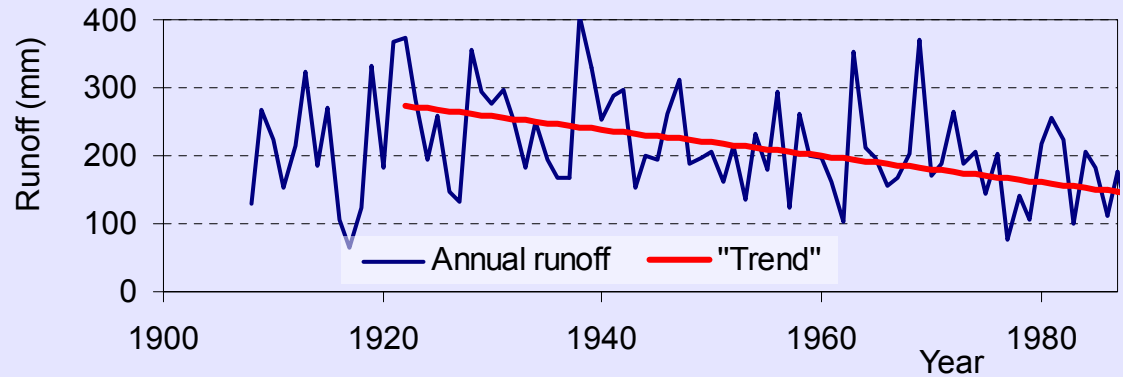
2. Hydrologic issues

2A. Diagnosis

Back in 1990s – Initial empirical observations

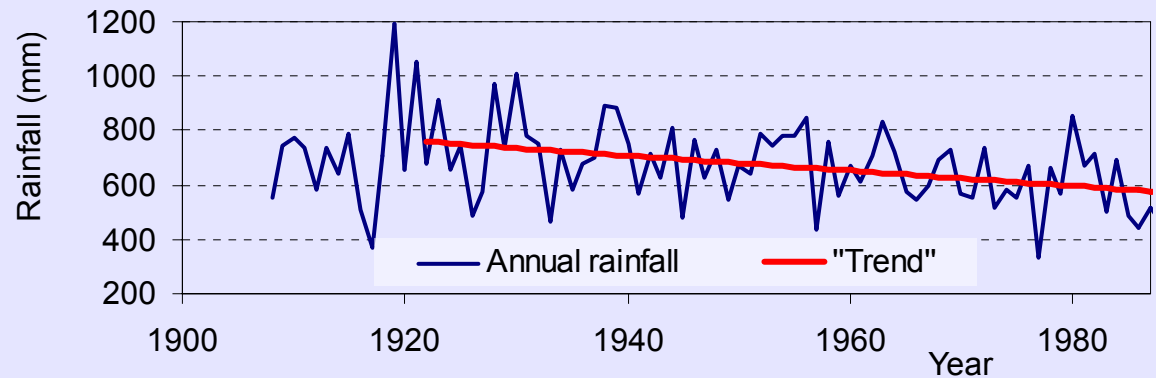
The historic time series of Boeotikos Kephisos runoff (Hydrologic years 1907/08-1986/87)

A multi-year «trend» is observed

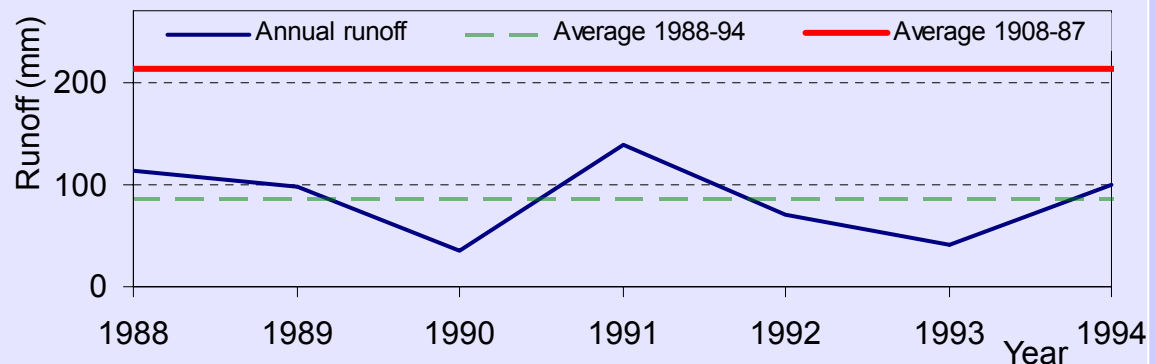


A similar «trend» in the rainfall time series

Explains the «trend» in runoff

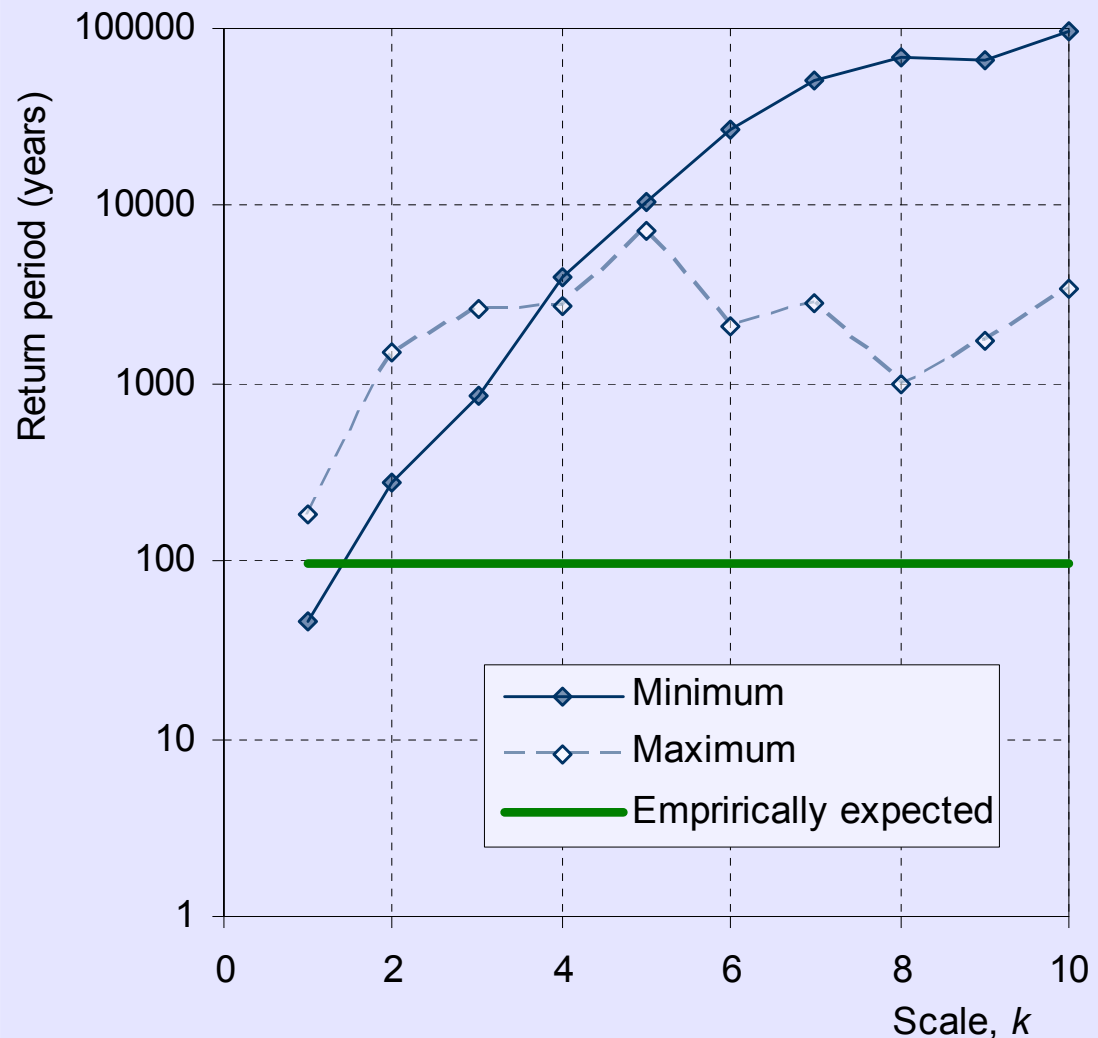


The next years were dry
Intense and persistent drought: Mean flow half that of the historic average, duration 7 years



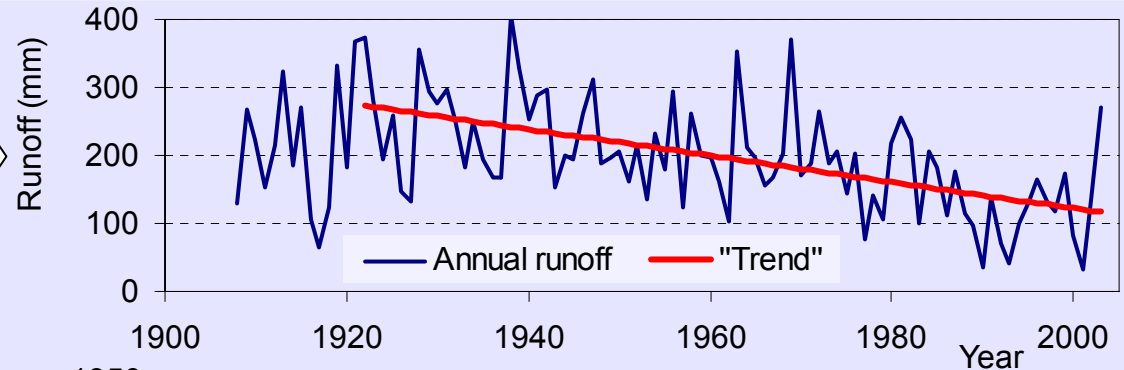
Return period of the persistent drought

- ◆ Assessment was done using classic hydrologic statistics
- ◆ At the annual scale, the drought was a record minimum but with typical magnitude
- ◆ Aggregated at larger scales, it appeared something extraordinary
- ◆ Similar behavior was observed for maxima on aggregate scales



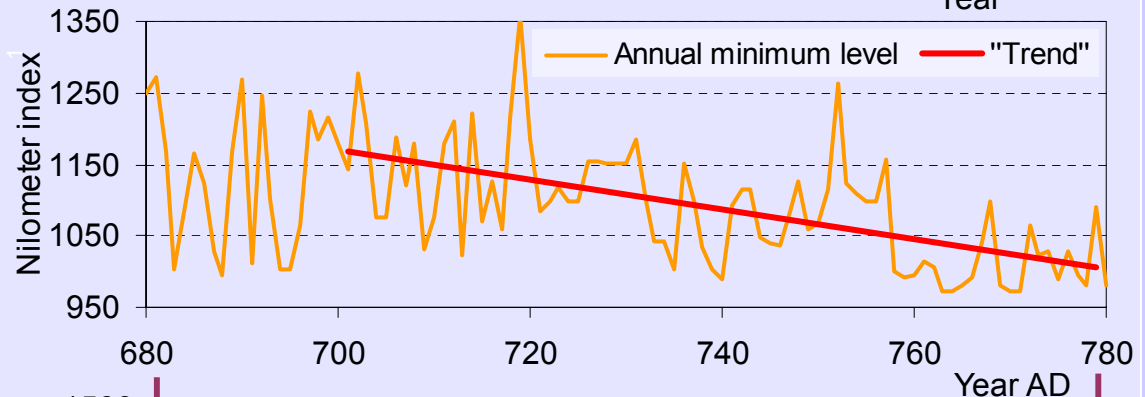
Comparisons with even longer series

The complete historic time series of Boeotikos Kephisos runoff



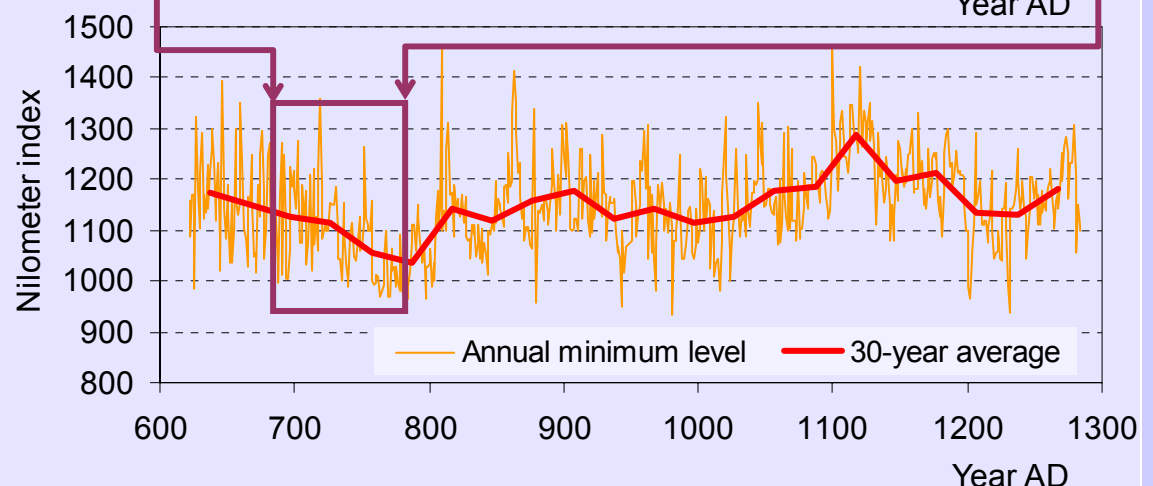
A part of the Nilometer series (an index of the minimum annual level in the Nile River*)

A similar «trend»



The complete Nilometer series (622-1284 AD, 663 years)

Upward and downward fluctuations on all scales



* J. Beran (1994), *Statistics for Long-Memory Processes*, Chapman & Hall, New York, USA

The fluctuations on many scales and the “Hurst phenomenon”

- ◆ The “weird” (as compared to purely random processes) behavior of hydrologic and other geophysical processes was discovered by the English engineer E. H. Hurst* (1950) in the framework of the design of the High Aswan Dam in Nile ⇒ **Hurst phenomenon**
- ◆ The Polish-French mathematician and engineer B. Mandelbrot (1965-1971) related it to the biblical story of the seven fat and the seven thin cows ⇒ **Joseph effect**
- ◆ The behavior has been characterized with several other names ⇒ **long-term persistence, long-term memory, long-range dependence**
- ◆ Most of these names, even though correct, may be misleading for the conceptualization and understanding of the natural behavior and the causing mechanisms. Probably a better name ⇒ **multi-scale fluctuation**
- ◆ The behavior was verified to be omnipresent, not only in geophysical processes (hydrologic, climatic), but also in biological (e.g. tree rings), technological (e.g. computer networks), social and economical (e.g. stock market)
- ◆ In water resources design and management, it has unfavorable effects (increase of uncertainty)

* H. E. Hurst (1950), Long-Term Storage Capacity of Reservoirs, *Proc. American Society of Civil Engineers*, 76(11)

Easy detection and main effect of Hurst phenomenon

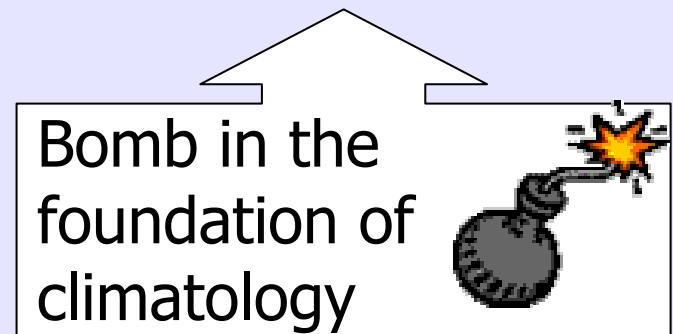
- ◆ Fundamental law of classic statistics $\text{StD}[\bar{X}_n] = \frac{\sigma}{\sqrt{n}}$
 - \bar{X}_n = average of n variables
 - σ = standard deviation of each variable
 - n = aggregation scale (or sample size)

- ◆ Modified law traced natural processes $\text{StD}[\bar{X}_n] = \frac{\sigma}{n^{1-H}}, H > 0.5$

- ◆ Example

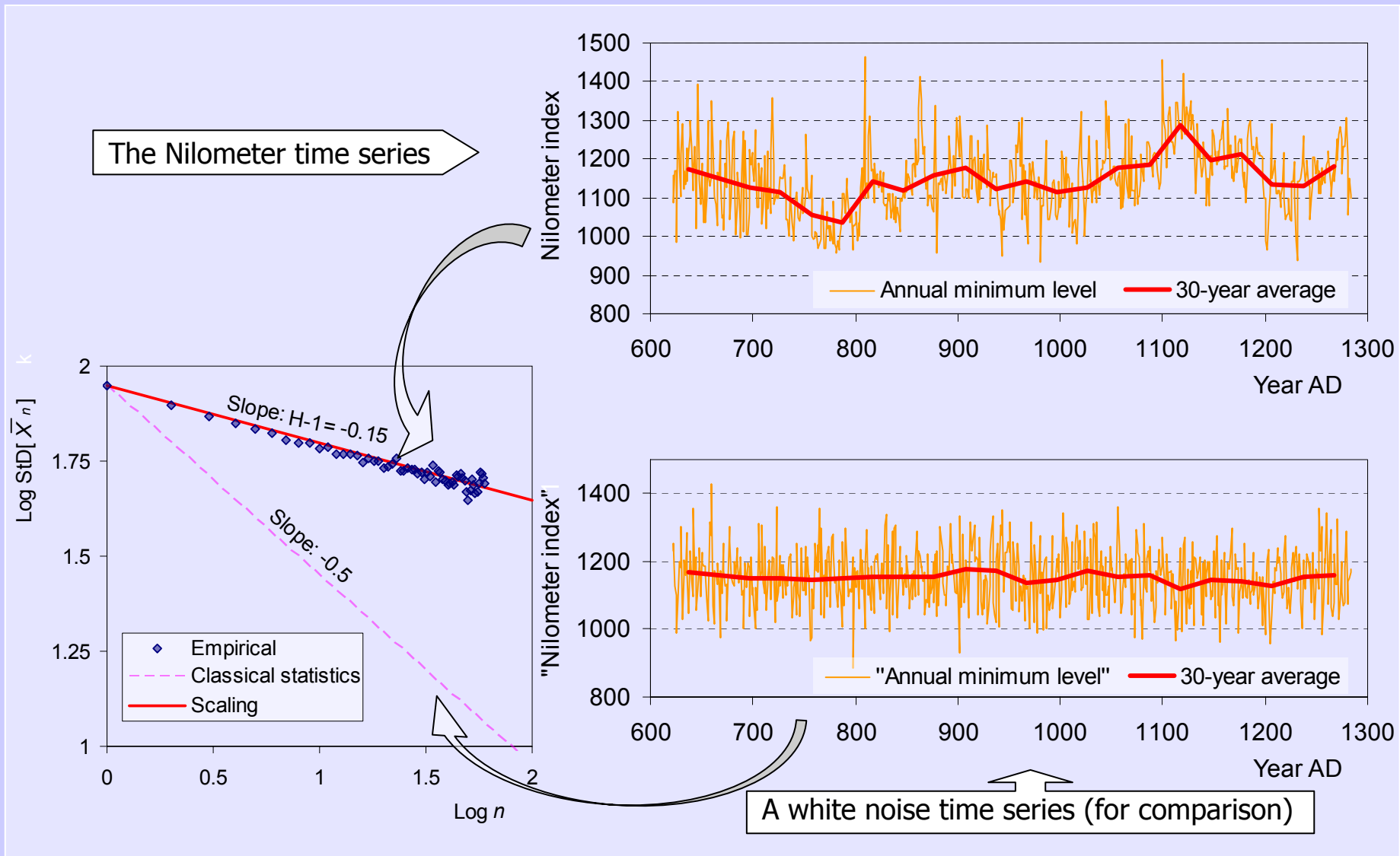
To have $\text{StD}[\bar{X}_n] / \sigma = 10\%$

- $n = 30$ in classic statistics
- $n = 5\,000$ for the modified law with $H = 0.8$



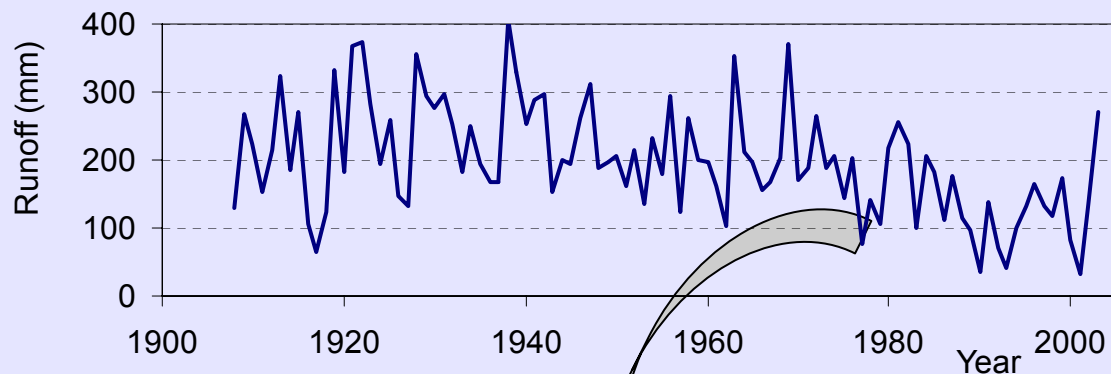
Incongruity of natural processes with typical random processes :

(a) The Nilometer series

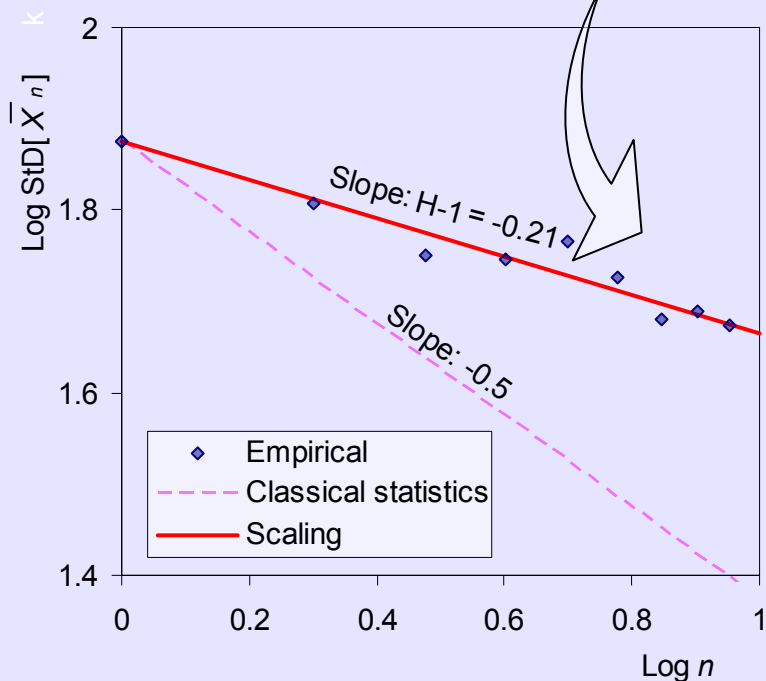


Incongruity of natural processes with typical random processes :

(b) The Boeotikos Kephisos time series



The time series of the Boeotikos Kephisos runoff



Statistical characteristics of all processes

Sample statistic	Runoff (mm)	Rainfall (mm)	Temperature (°C)
n	96	96	96
m (mm)	197.6	658.4	17.0
s (mm)	87.6	158.9	0.72
C_s	0.36	0.44	0.34
r_1	0.34	0.10	0.31
H	0.79	0.64	0.72

Mathematical description of the Hurst phenomenon

- ◆ The mathematical description of the Hurst phenomenon is done on grounds of probability theory and particularly theory of stochastic process
- ◆ The simple relationship

$$\text{StD}[\bar{X}_n] = \frac{\sigma}{n^{1-H}}$$

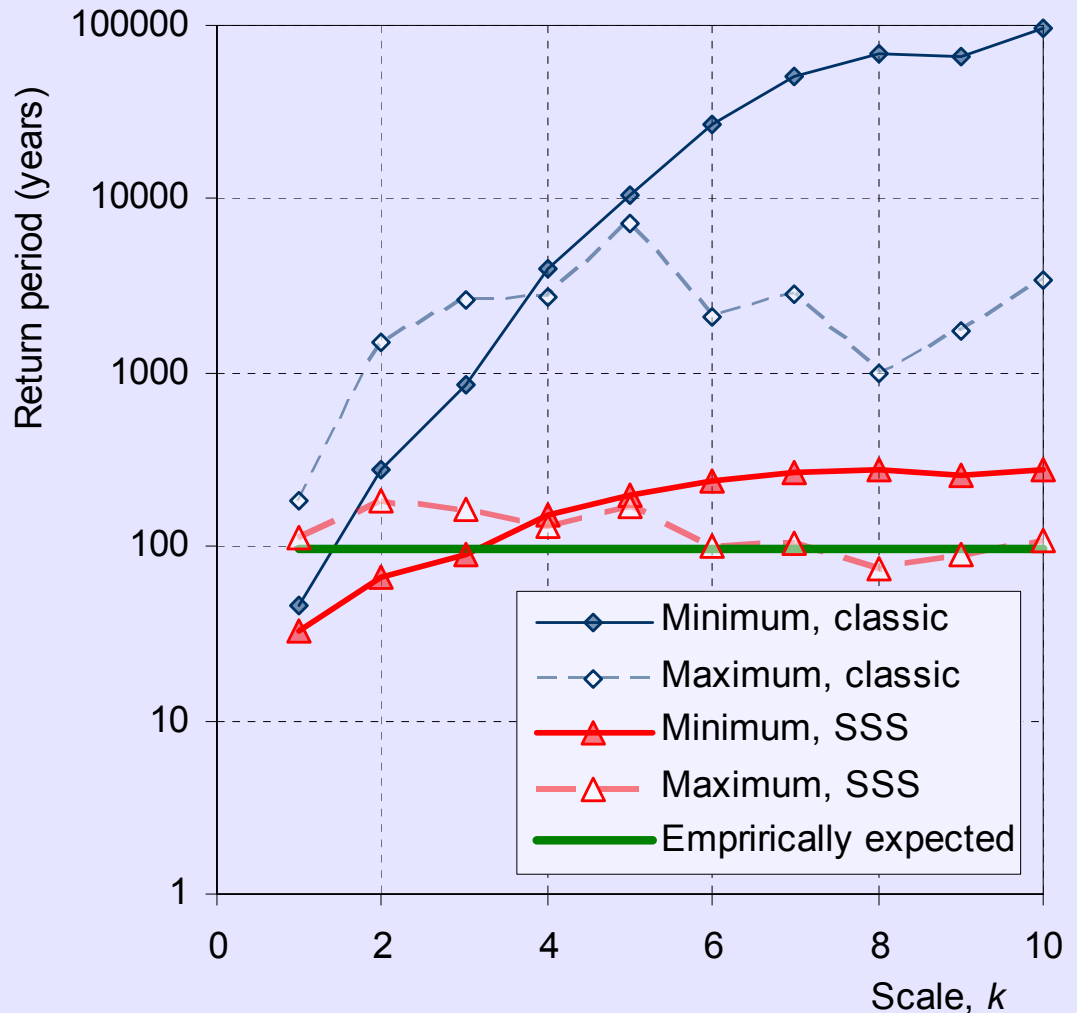
entails a definition (good for our purposes) of a model (stochastic process) reproducing the Hurst phenomenon; n is meant as a scale of aggregation (rather than sample size)

- ◆ (Hurst used a different formalism, in terms of the so called rescaled range, which is complicated and probably misleading)
- ◆ Today the stochastic process with the above property is called a **Self-Similar process with Stationary intervals** or a **Simple Scaling Stochastic process** (abbreviated as an **SSS process**)
- ◆ The SSS process was introduced by the Russian mathematician A. Kolmogorov* (1940) who called it **Wiener Spiral**
- ◆ A significant contribution on the SSS process is due to the American mathematician J. Lamperti (1962) who called it a **Semi-Stable Process**
- ◆ The link of the SSS process with the Hurst phenomenon is due to B. Mandelbrot (1965), who called it **Fractional Brownian Noise**

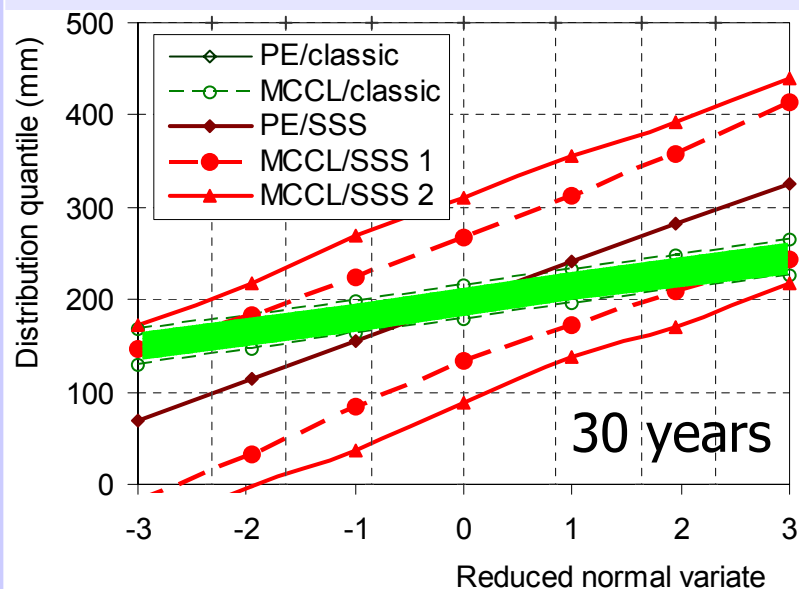
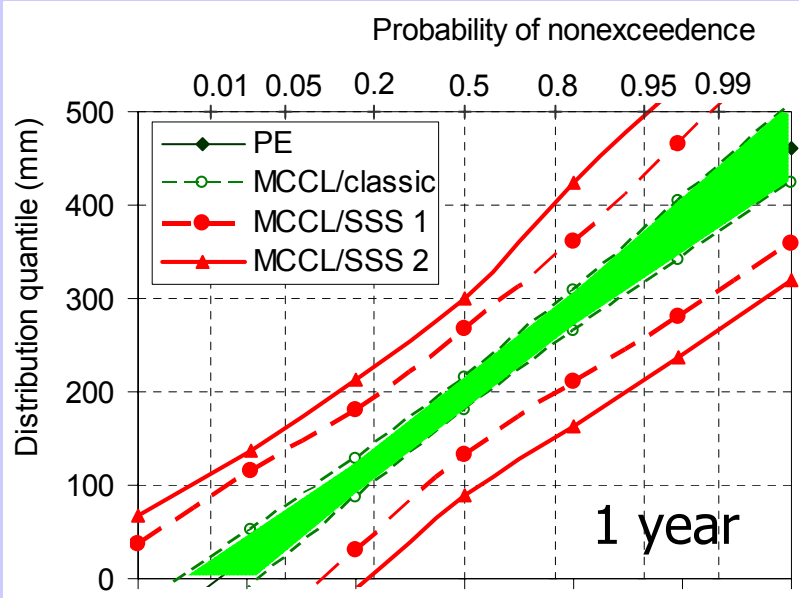
* A. N. Kolmogorov (1940), Wienersche Spiralen und einige andere interessante Kurven in Hilbertschen Raum, Comptes Rendus (Doklady) Acad. Sci. USSR (N.S.) 26, 115–118

Back to Boeotikos Kephisos – Adoption of the SSS process

- ◆ The trend is a natural and usual behavior
- ◆ The persistent drought is not extraordinary; it is a natural and expected behavior



Implications on uncertainty: Boeotikos Kephisos runoff



Statistical model	Total uncertainty in runoff (due to variability and parameter estimation) % of average	
	Annual scale	30-year scale
Classic	200	50
SSS	270	200

Classic model
Climate is what you expect
Weather is what you get

SSS model
Weather is what you get ... immediately
Climate is what you get
... if you keep expecting a long time

2. Hydrologic issues

2B. Explanation

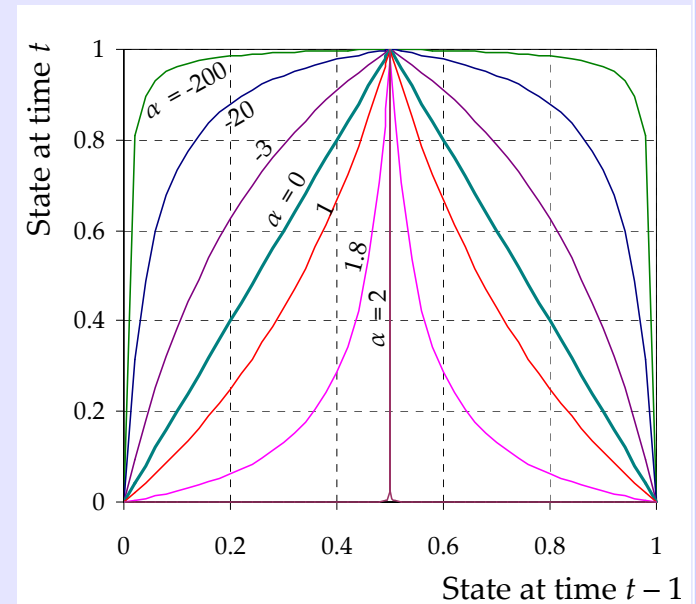
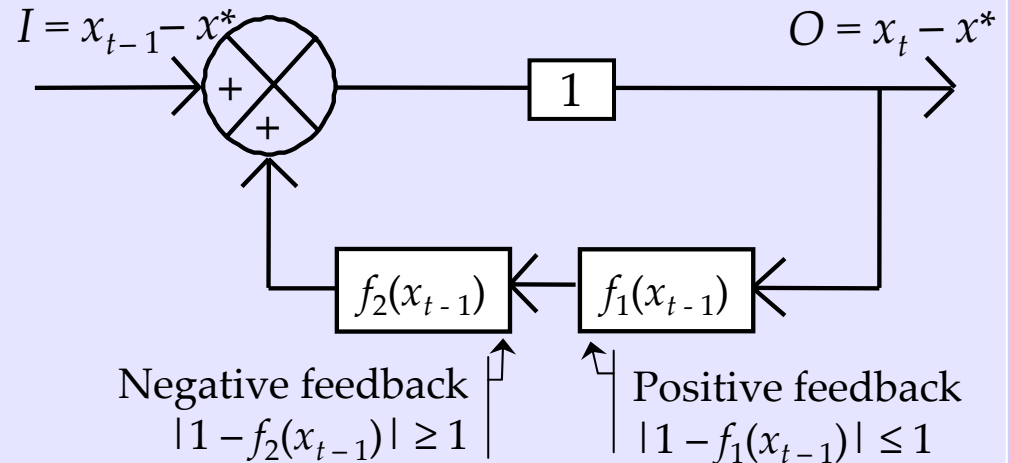
A climatic toy model: A simple system with nonlinear dynamics may produce the Hurst phenomenon

- ◆ A simplified climatic system is represented as a circuit with two feedback mechanisms, a positive (amplifying the departure from a stationary state x^*) and a negative (reducing this departure)
- ◆ The combined action of the two mechanisms could be represented by a generalized tent transform:

$$x_t = \frac{(2 - \alpha) \min(x_{t-1}, 1 - x_{t-1})}{1 - \alpha \min(x_{t-1}, 1 - x_{t-1})}$$

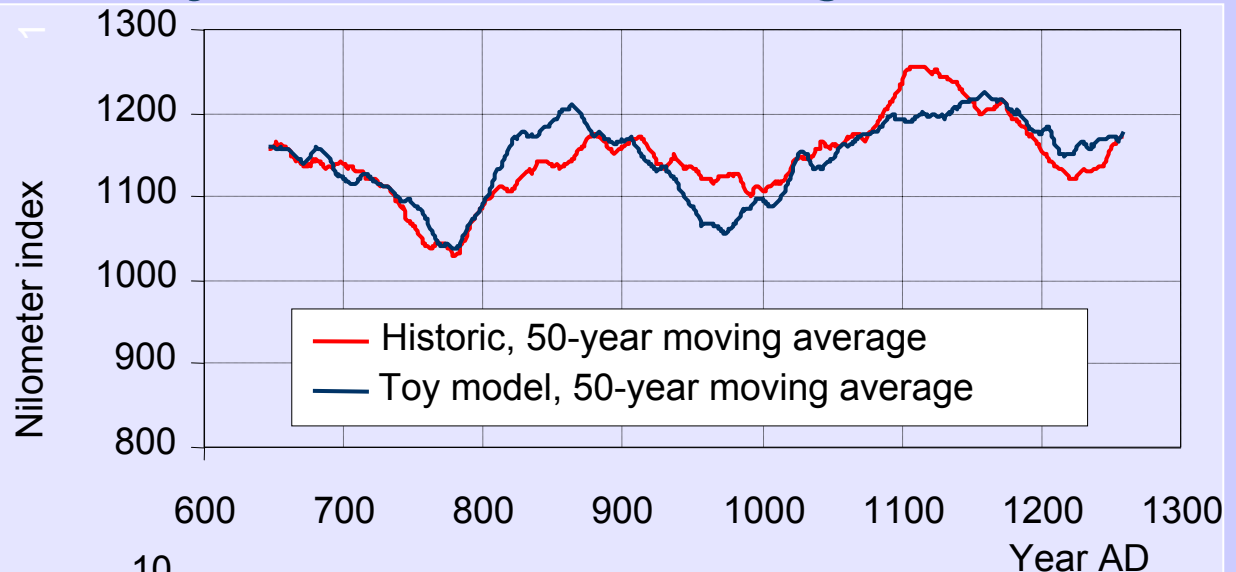
where $0 \leq x_t \leq 1$, $\alpha < 2$

- ◆ The parameter α could be assumed to vary in time, following the same tent transform with a constant parameter β

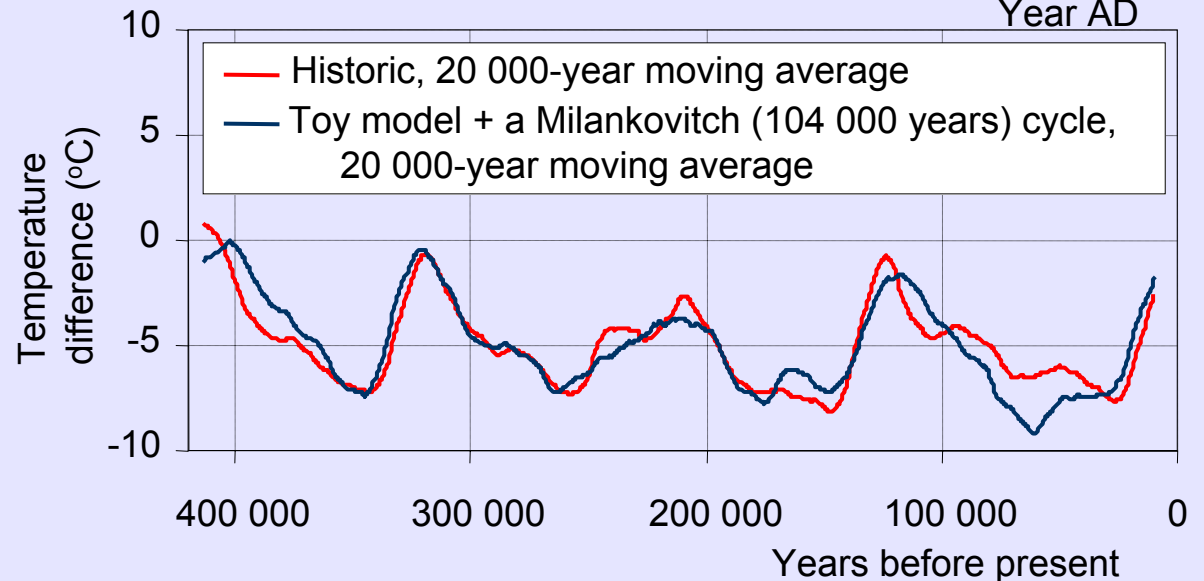


Demonstration continued: Toy model fitted to two long time series

The Nilometer time series

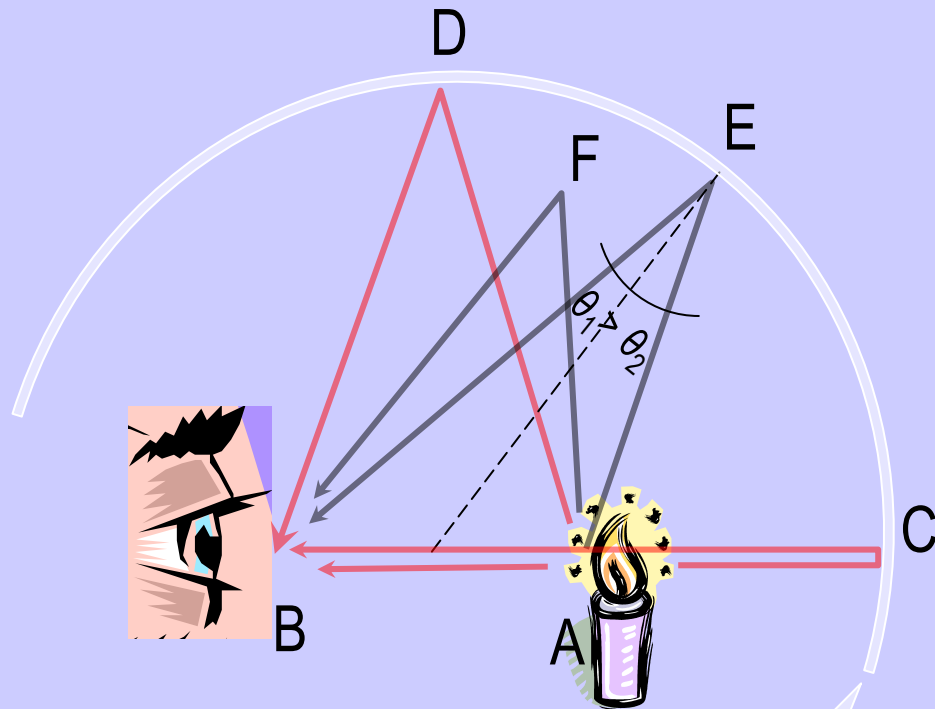


The Vostok (Antarctica) ice core deuterium data set going back to 422 766 years before present*
Reconstructed temperature difference with reference to the mean recent time value



* Petit J.R., Jouzel J., Raynaud D., Barkov N.I., Barnola J.M., Basile I., Bender M., Chappellaz J., Davis J., Delaygue G., Delmotte M., Kotlyakov V.M., et al., Climate and atmospheric history of the past 420,000 years from the Vostok ice core, Antarctica, *Nature*, 399, 429-436, 1999.

Towards a more general explanation: Nature loves extremes ...



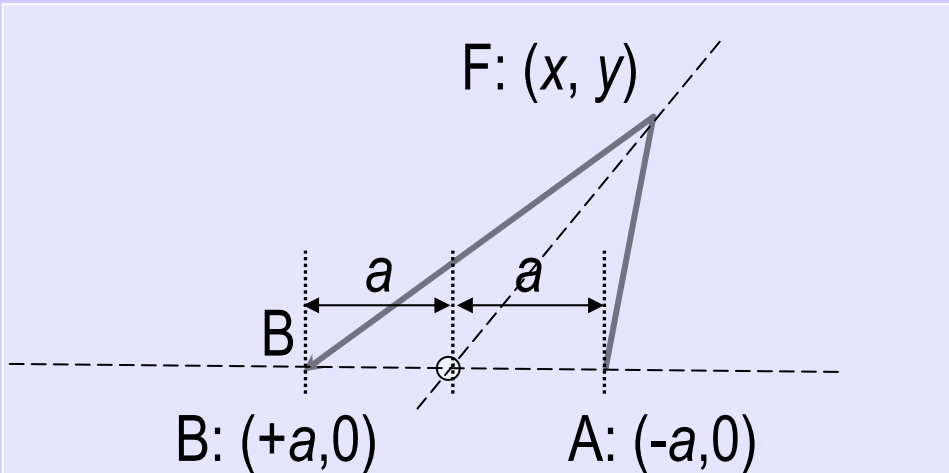
A semi-cylindrical mirror

Why light follows the red paths from A to B (AB, ACB, ADB) and not other (the black) ones (e.g. AEB, AFB)?

- The red paths are those that (a) reach the mirror and (b) form an angle of incidence equal to the angle of reflection
(True for most cases; not true for AB; not general or informative)
- The red paths have minimum travel time (or length)
(Not true for ADB)
- The red paths have extreme (minimum or maximum) travel time (or length)

(True)

The light example – no mirror

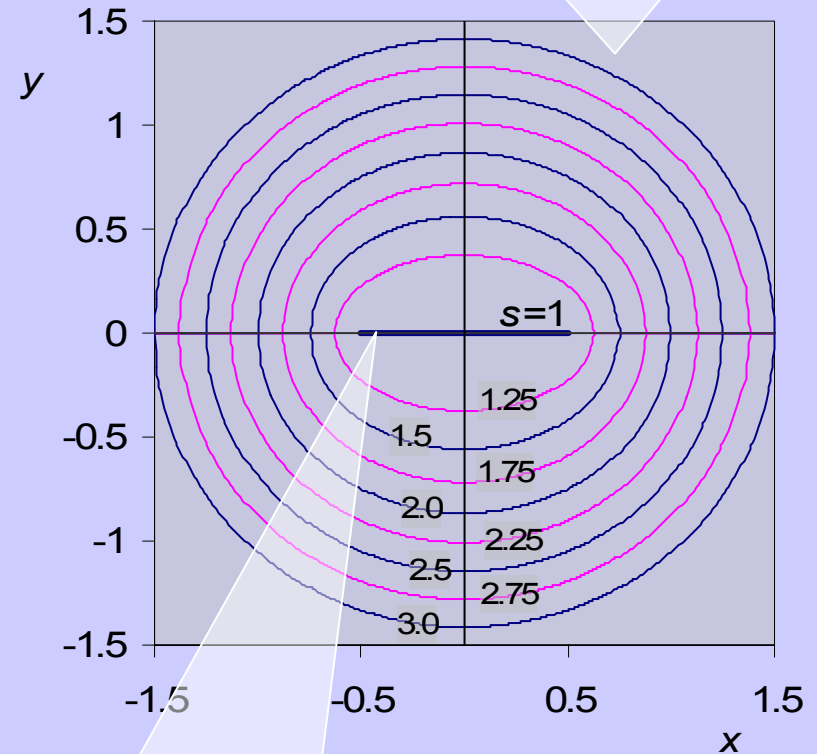


Assume that light can travel from A to B along a broken line with a break point F with coordinates (x, y) .
 (This is not restrictive: later we can add a second, third, ... break points)
 The travel distance is $s(x, y) = AF + FB$ where

$$AF = \sqrt{(x - a)^2 + y^2}$$

$$FB = \sqrt{(x + a)^2 + y^2}$$

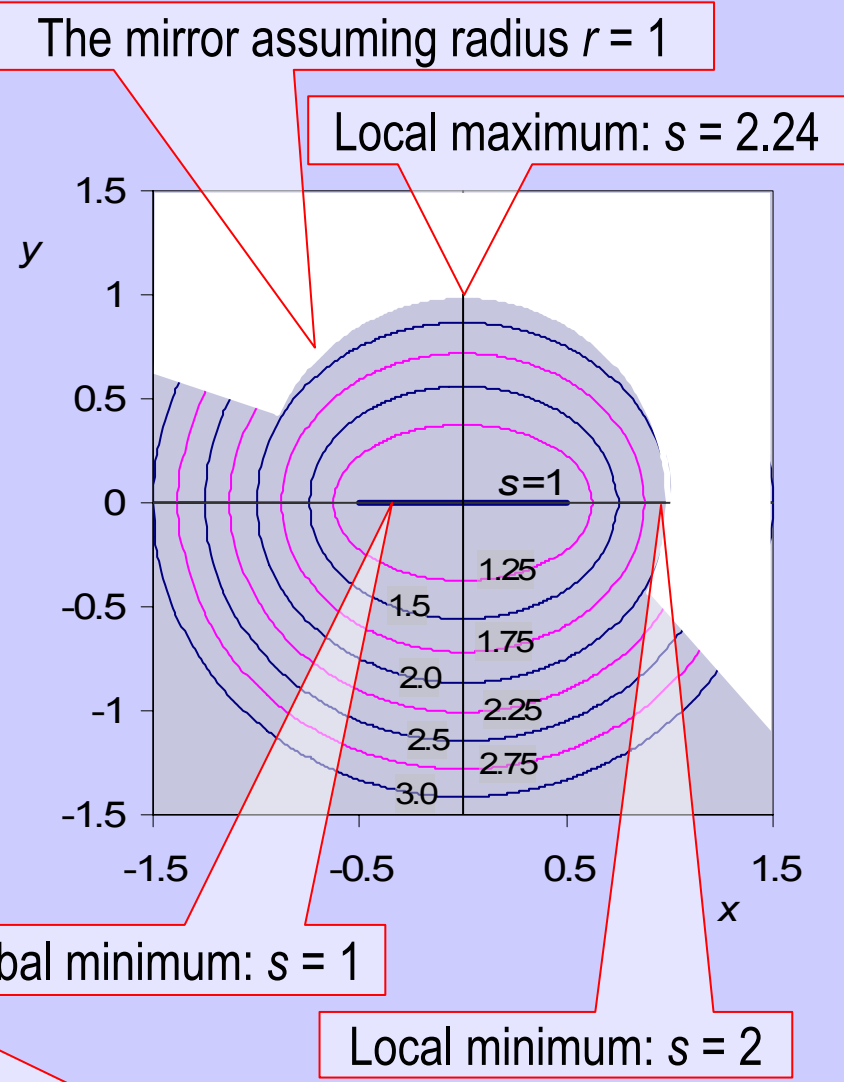
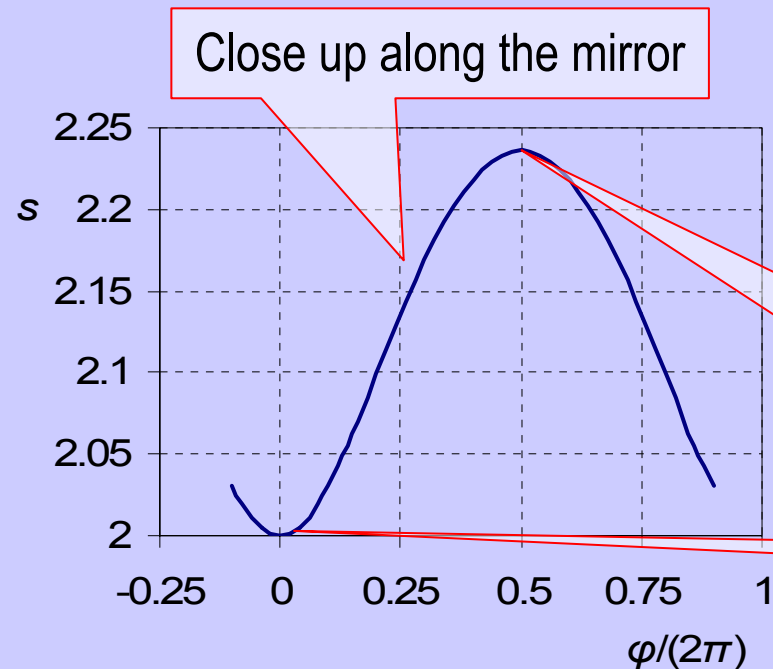
Contours of the distance $s(x, y)$ assuming $a = 0.5$



Line of minimum distance $s(x, y) = 1$
 Infinite points F essentially describing the same path

The light example with mirror

- ◆ The mirror introduces an inequality constraint in the optimization: the point F should not be behind the mirror
- ◆ Two points of local optima emerge on the mirror surface (the curve where the constraint is binding)



Local maximum: $s = 2.24$

Local minimum: $s = 2$

How nature works? (a hypothesis ...)

Property

- ◆ She preserves a few quantities
(mass, momentum energy,)
- ◆ She optimizes a single quantity
(Dependent on the specific system -
Difficult to find what this quantity is)
- ◆ She disallows some states
(Dependent on the specific system –
Maybe difficult to find)

Mathematical formulation

- ◆ One equation per preserved quantity:

$$g_i(\mathbf{s}) = c_i, \quad i = 1, \dots, k$$

where c_i constants; \mathbf{s} the size n vector of state variables ($n \geq k$, sometimes $n = \infty$)

- ◆ A single “optimization”:

$$\text{optimize } f(\mathbf{s})$$

[i.e. maximize/minimize $f(\mathbf{s})$] **This is equivalent to many equations** (as many as required to determine \mathbf{s})

Conversely, many equations can be combined into an “optimization”

- ◆ Inequality constraints:

$$h_j(\mathbf{s}) \geq 0, \quad j = 1, \dots, m$$

- ◆ In conclusion, we may find how nature works solving the problem:

$$\text{optimize } f(\mathbf{s})$$

$$\text{s.t. } g_i(\mathbf{s}) = c_i, \quad i = 1, \dots, k$$

$$h_j(\mathbf{s}) \geq 0, \quad j = 1, \dots, m$$

The typical “optimizable” quantity in complex systems ...

- ◆ ... is entropy – entropie – Entropie – entropia – entropía – entropi – entrópia – entroopia – entropija – энтропия – ентропія – 熵 – エントロピー – س مقیاس – אנטרופיה – εντροπία
- ◆ The word is ancient Greek (εντροπία, a feminine noun meaning: turning into; turning towards someone’s position; turning round and round)
- ◆ The scientific term is due to Clausius (1850)
- ◆ The entropy concept was fundamental to formulate the second law of thermodynamics
- ◆ Boltzmann (1877), then complemented by Gibbs (1948), gave it a statistical mechanical content, showing that entropy of a macroscopical stationary state is proportional to the logarithm of the number w of possible microscopical states that correspond to this macroscopical state
- ◆ Shannon (1948) generalized the mathematical form of entropy and also explored it further. At the same time, Kolmogorov (1957) founded the concept on more mathematical grounds on the basis of the measure theory

What is entropy?

- ◆ Entropy is defined on grounds of probability theory
- ◆ For a discrete random variable X taking values x_j with probability mass function $p_j \equiv p(x_j)$, $j = 1, \dots, w$, the Boltzmann-Gibbs-Shannon (or extensive) entropy is defined as

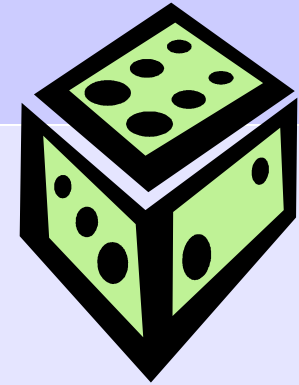
$$\varphi := E[-\ln p(X)] = -\sum_{j=1}^w p_j \ln p_j, \quad \text{where } \sum_{j=1}^w p_j = 1$$

- ◆ For a continuous random variable X with probability density function $f(x)$, the entropy is defined as

$$\varphi := E[-\ln f(X)] = -\int_{-\infty}^{\infty} f(x) \ln f(x) dx, \quad \text{where } \int_{-\infty}^{\infty} f(x) dx = 1$$

- ◆ In both cases the entropy φ is a measure of **uncertainty** about X and equals the **information** gained when X is observed.
- ◆ In other disciplines (statistical mechanics, thermodynamics, dynamical systems, fluid mechanics), entropy is regarded as a measure of **order** or **disorder** and **complexity**.
- ◆ Generalizations of the entropy definition have been introduced more recently (Renyi, Tsallis)

Entropy maximization: The die example



◆ What is the probability that the outcome of a toss of a die will be i ? ($i = 1, \dots, 6$)

◆ The entropy is:

$$\varphi := E[-\ln p(X)] = -p_1 \ln p_1 - p_2 \ln p_2 - \dots - p_6 \ln p_6$$

◆ The equality constraint (mass preservation) is

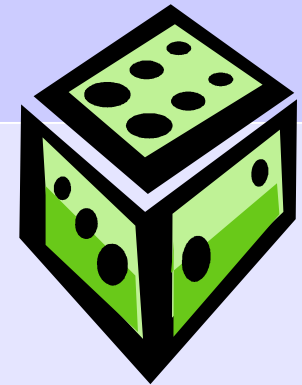
$$p_1 + p_2 + \dots + p_6 = 1$$

◆ The inequality constraint is $p_i \geq 0$

◆ Solution of the optimization problem (e.g. by the Lagrange method) yields a single maximum: $p_1 = p_2 = \dots = p_6 = 1/6$

◆ This method, the application of the Maximum Entropy Principle (mathematically, an “optimization” form) is equivalent to the Principle of Insufficient Reason (Bernoulli-Laplace; mathematically, an “equation” form)

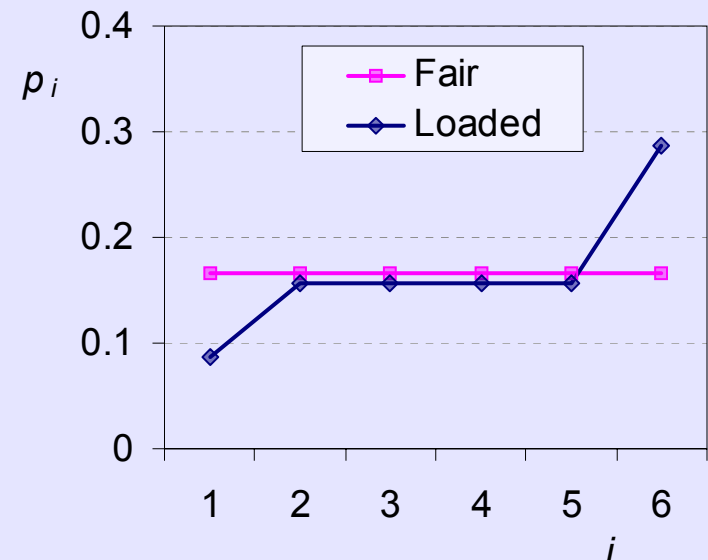
Entropy maximization: The loaded die example



- ◆ What is the probability that the outcome of a toss of a die will be i ($i = 1, \dots, 6$) if we know that it is loaded, so that $p_6 - p_1 = 0.2$?
- ◆ The IS principle does not work in this case
- ◆ The ME principle works. We simply pose an additional constraint:

$$p_6 - p_1 = 0.2$$

- ◆ The solution of the optimization problem (e.g. by the Lagrange method) is a single maximum:



Entropy maximization: The temperature example

- ◆ What will be the temperature in my house (T_H), compared to that of the environment (T_E)? (Assume an open window and no heating equipment)
- ◆ Take a space of environment (E) in contact to the house (H) with volume equal to that of the house
- ◆ Partition the continuous range of kinetic energy of molecules into several classes $i = 1$ (coldest), 2, ..., k (hottest)
- ◆ Denote p_i the probability that a molecule belongs to class i , and partition it to p_{Hi} and p_{Ei} , if the molecule is in the house or the environment, respectively
- ◆ Form the entropy in terms of p_{Hi} and p_{Ei}
- ◆ Maximize entropy conditional on $p_{Hi} + p_{Ei} = p_i$
- ◆ The result is $p_{Hi} = p_{Ei}$
- ◆ Equal number of molecules of each class are in the house and the environment, so $T_H = T_E$
- ◆ This could be obtained also from the IR principle



Formalization of the principle of maximum entropy

- ◆ In a probabilistic context, the principle of ME was introduced by Janes (1957)
- ◆ In a probabilistic context, the principle of ME is used to infer unknown probabilities from known information
- ◆ In a physical context, it determines thermodynamical states
- ◆ The principle postulates that the entropy of a random variable should be at maximum, under some conditions, formulated as constraints, which incorporate the information that is given about this variable
- ◆ Typical constraints used in a probabilistic or physical context are:

Mass

$$\int_{-\infty}^{\infty} f(x) dx = 1,$$

Mean/Momentum

$$E[X] = \int_{-\infty}^{\infty} x f(x) dx = \mu$$

Non-negativity

$$x \geq 0$$

Variance/Energy

$$E[X^2] = \int_{-\infty}^{\infty} x^2 f(x) dx = \sigma^2 + \mu^2,$$

Dependence/Stress

$$E[X_i X_{i+1}] = \int_{-\infty}^{\infty} x_i x_{i+1} f(x_i, x_{i+1}) dx_i dx_{i+1} = \rho \sigma^2 + \mu^2$$

Some results of ME interesting to hydrology

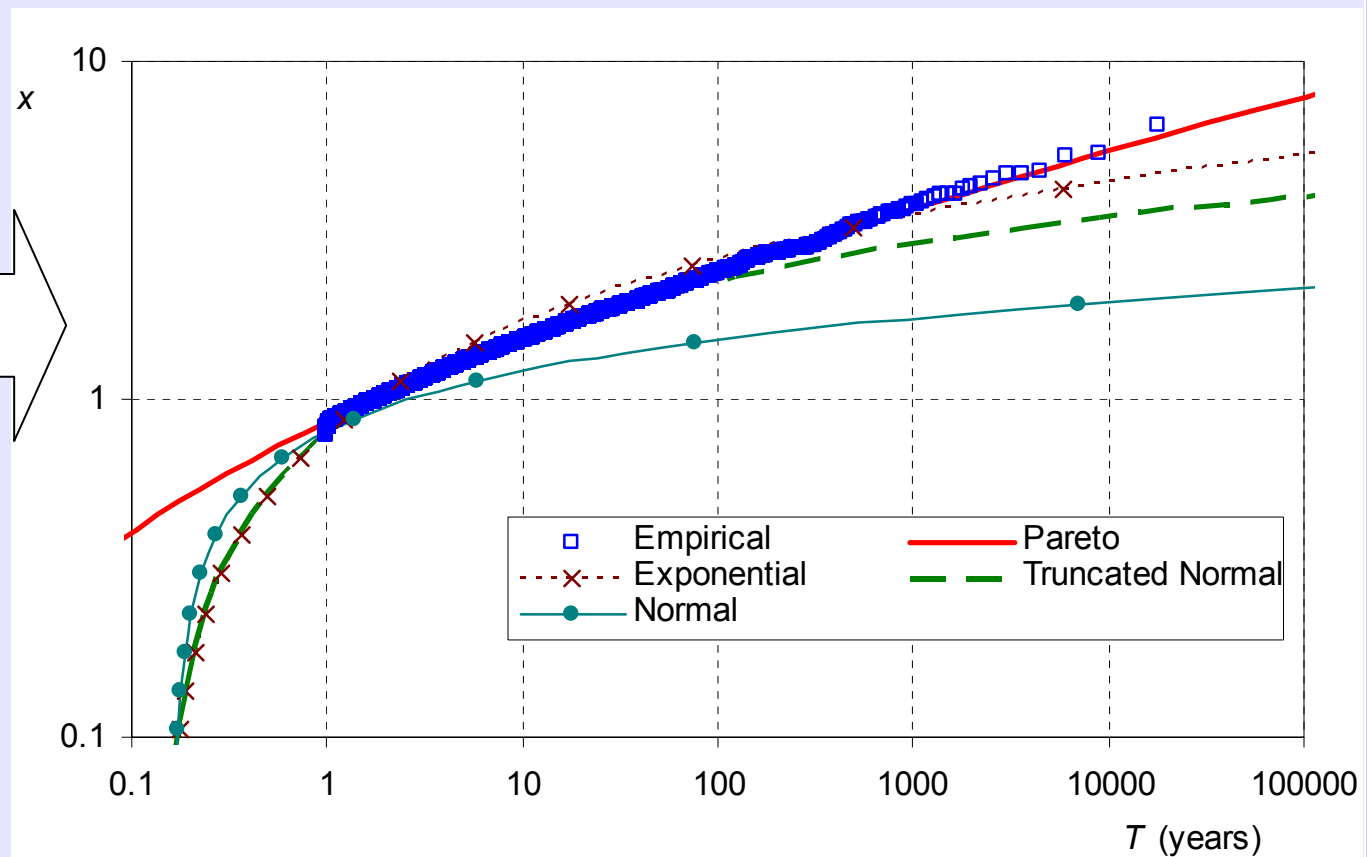
- ◆ Assume that a hydrometeorological variable X (e.g. temperature, rainfall, runoff) is continuous and positive, has known mean μ and known variation σ/μ . Estimate the distribution function with only this information, applying the ME principle
- ◆ The results are:
 - Maximum entropy + Low variation \rightarrow (Truncated) normal distribution
 - Maximum entropy + High variation \rightarrow Power-type (Pareto) distribution
 - Maximum entropy + High variation + High return periods \rightarrow State scaling
- ◆ The celebrated state scaling ($x_T \sim T^K$, where T is the return period and x_T the corresponding quantile) is only:
 - ◆ a consequence of the ME principle,
 - ◆ an approximation, good for high return periods and for variables with high variation
- ◆ Real world time series (especially long ones) validate the applicability of the ME principle in hydrometeorological processes

ME application to extreme daily rainfall worldwide

Data set: Daily rainfall from 168 stations worldwide each having at least 100 years of measurements; series above threshold, standardized by mean and unified; period 1822-2002; 17922 station-years of data

$\mu = 0.28$
(mean minus
threshold)
 $\sigma/\mu = 1.19 > 1$
ME distribution:
Pareto
 $\kappa = 0.15$
 $\varphi_q = 1.16$

Conclusion:
Scaling
for $T > \sim 50$ yr



Entropic quantities of a stochastic process

- ◆ The *order 1 entropy* (or simply *entropy* or *unconditional entropy*) refers to the marginal distribution of the process X_i :

$$\varphi := E[-\ln f(X_i)] = - \int_{-\infty}^{\infty} f(x) \ln f(x) dx, \quad \text{where } \int_{-\infty}^{\infty} f(x) dx = 1$$

- ◆ The *order n entropy* refers to the joint distribution of the vector of variables $\mathbf{X}_n = (X_1, \dots, X_n)$ taking values $\mathbf{x}_n = (x_1, \dots, x_n)$:

$$\varphi_n := E[-\ln f(\mathbf{X}_n)] = - \int_{D_n} f(\mathbf{x}_n) \ln f(\mathbf{x}_n) d\mathbf{x}_n$$

- ◆ The *order m conditional entropy* refers to the distribution of a future variable (for one time step ahead) conditional on known m past and present variables (Papoulis, 1991):

$$\varphi_{c,m} := E[-\ln f(X_1 | X_0, \dots, X_{-m+1})] = \varphi_m - \varphi_{m-1}$$

- ◆ The *conditional entropy* refers to the case where the entire past is observed:

$$\varphi_c := \lim_{m \rightarrow \infty} \varphi_{c,m}$$

- ◆ The *information gain* when present and past are observed is:

$$\psi := \varphi - \varphi_c$$

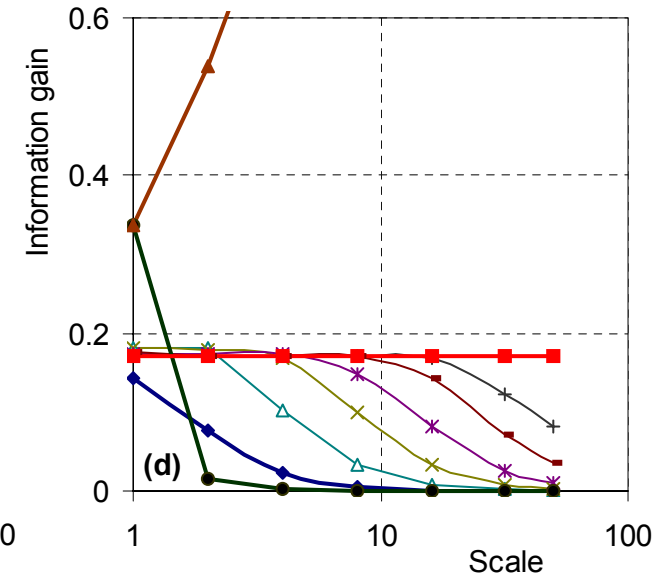
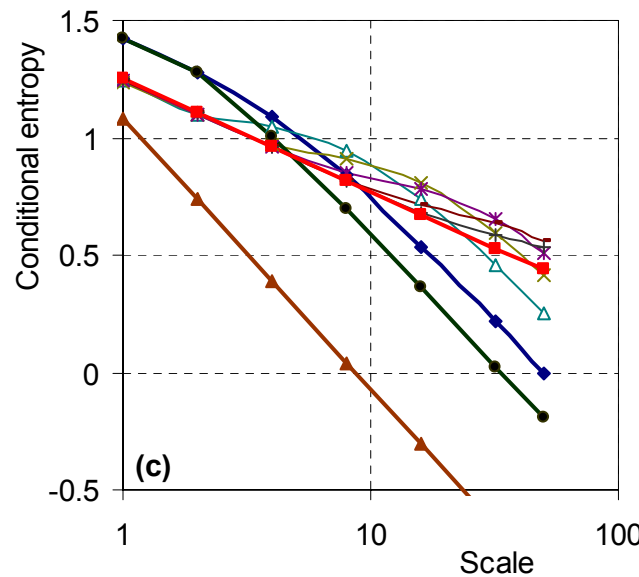
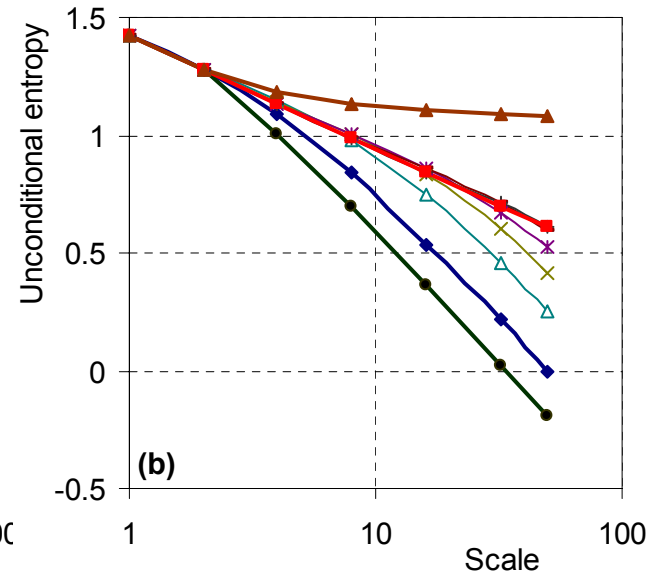
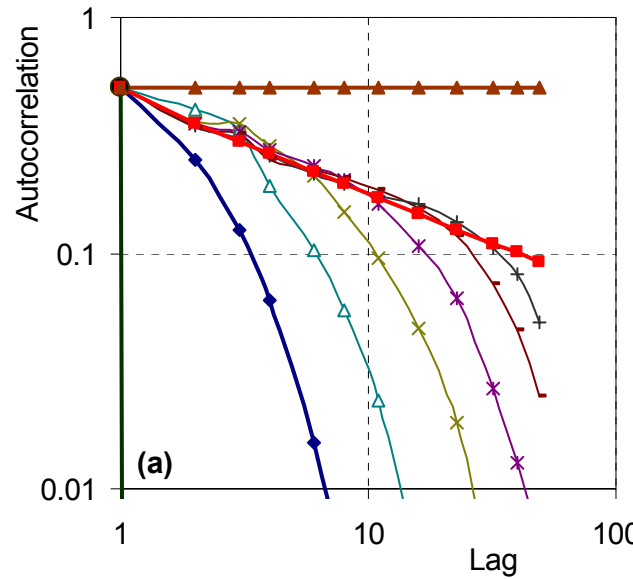
Note: notation assumes stationarity

Entropy maximization for a stochastic process

- ◆ The purpose is to determine not only marginal probabilities but the dependence structure as well
- ◆ All five constraints are used (mass/mean/variance/dependence/non-negativity)
- ◆ The lag one autocorrelation (used in the dependence constraint) is determined for the basic (annual) scale but the entropy maximization is done on other scales as well
- ◆ The variation is low ($\sigma/\mu \ll 1$) and thus the process is virtually Gaussian (intermediate result). This is valid for annual and over-annual time scales
- ◆ For a Gaussian process the n th order entropy is given as $\varphi_n = \ln \sqrt{(2\pi e)^n \delta_n}$ where δ_n is the determinant of the autocovariance matrix $c_n := \text{Cov}[\mathbf{X}_n, \mathbf{X}_n]$.
- ◆ The autocovariance function is assumed unknown to be determined by application of the ME principle. Additional constraints for this are:
 - Mathematical feasibility, i.e. positive definiteness of c_n (positive δ_n)
 - Physical feasibility, i.e. autocorrelation function (a) positive and (b) non increasing with lag and time scale
(Note: periodicity that may result in negative autocorrelations is not considered here due to annual and over-annual time scales)

Demonstration: Maximization of unconditional entropy averaged over ranges of scales

Conclusion:
As the range of
time scales widens,
the dependence
tends to SSS



- △— Scales 1-4 —×— Scales 1-8
- *— Scales 1-16 —■— Scales 1-32
- +— Scales 1-50 —●— MA
- ◆— AR —■— FGN
- ▲— GN

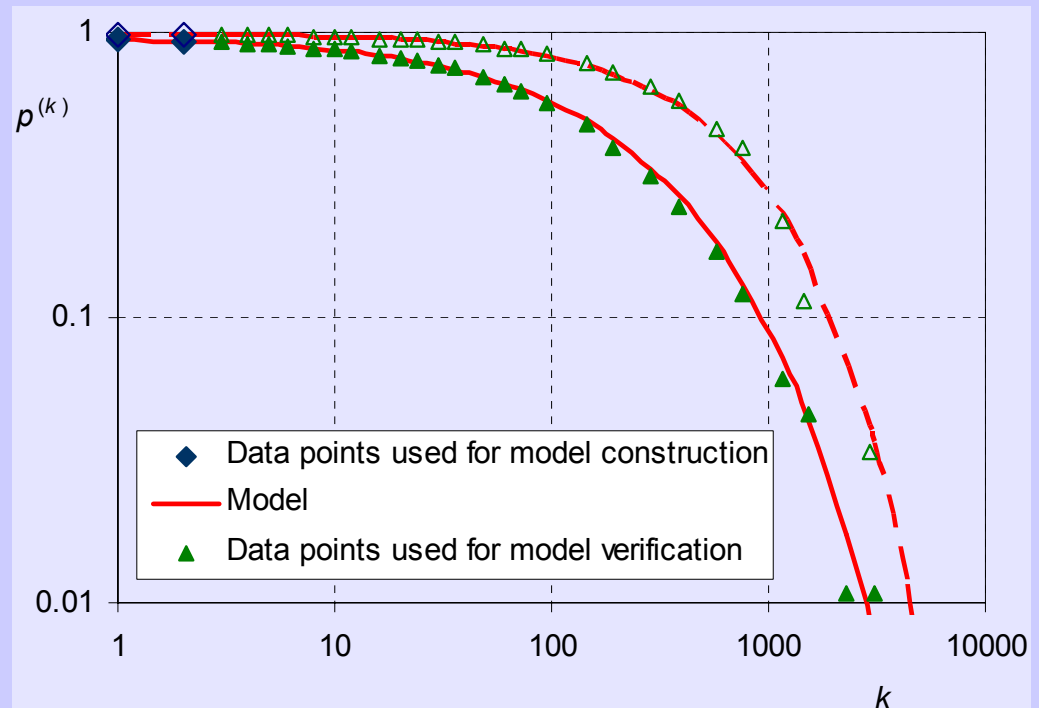
Results of the ME principle in stochastic processes

- ◆ Maximum entropy + Low variation + Dominance of a single time scale → Normal distribution + Time independence
- ◆ Maximum entropy + Low variation + Time dependence + Dominance of a single time scale → Normal distribution + Markovian (short-range) time dependence
- ◆ Maximum entropy + Low variation + Time dependence + Equal importance of time scales → Normal distribution + Time scaling (long-range dependence / Hurst phenomenon)
- ◆ The time scaling behavior is a result of the principle of maximum entropy
- ◆ The omnipresence of time scaling in numerous long hydrologic time series, validates the applicability of the ME principle

Another peculiar dependence explained by ME

- ◆ Rainfall at small scales is intermittent
- ◆ The dependence of the rainfall occurrence process is not Markovian neither scaling but in between; it has been known as clustering or overdispersion
- ◆ The models used for the rainfall occurrence process (point processes) are essentially those describing clustering of stars and galaxies
- ◆ The ME principle applied with the binary state rainfall process in more or less the same way as in the continuous state process explains this dependence

Probability $p^{(k)}$ that an interval of k hours is dry, as estimated from the Athens rainfall data set and predicted by the model of maximum entropy for the entire year (full triangles and full line) and the dry season (empty triangles and dashed line)



Interpretation of results

- ◆ The successful application of the ME principle in nature offers an explanation for of a plethora of phenomena (e.g. thermodynamic) and statistical behaviors including
 - the emergence of normal distribution, in many (but not all) cases
 - the scaling behavior in state, in other cases
 - the scaling behavior in time
 - the clustering behavior in rainfall occurrence
- ◆ This can be interpreted as dominance of uncertainty or ignorance in nature
- ◆ It harmonizes with the Socratic view: «Ἔν οἶδα, ὅτι οὐδέν οἶδα» (One I know, that I know nothing)
- ◆ This view was not a confession of modesty – Socrates regarded the knowledge of ignorance as a matter of supremacy
- ◆ In this respect, the knowledge of the dominance of uncertainty can assist to safer design and management of hydrosystems

2. Hydrologic issues

2C. Operational synthesis

Stochastic simulation/forecasting of hydrologic processes

◆ Question: Why simulated series?

◆ Answer:

- Analytical solutions for a hydrosystem as complex as that of Athens are not feasible or would assume oversimplification of the system
- Of numerical methods, Monte Carlo simulation (stochastic simulation) is the most convenient
- Detailed inflow and other (rainfall, evaporation) hydrologic series are needed at many sites simultaneously and at several time scales for Monte Carlo simulation the hydrosystem
- The acceptable failure probability level for Athens is of the order of 10^{-2} : one failure in 100 years on the average
- For a reasonable estimation error in the failure probability we need 1000-10 000 years of data
- Historic hydrologic records are too short

Requirements for stochastic simulation

1. Multivariate model
2. Multiple time scales of operation: annual to monthly or sub-monthly
3. Multiple time scales of preservation: multi-year (reproduction of the Hurst phenomenon) to sub-monthly (reproduction of sub-annual periodicity)
4. Preservation of essential marginal statistics up to third order (skewness)
5. Preservation of joint second order statistics
 - ◆ autocorrelations of any type and any lag
 - ◆ concurrent cross-correlations
6. Parsimony of parameters
7. Performance in simulation mode (steady state simulations) and in forecast mode, given the current and historic values (terminating simulations)

Models with such features did not exist (particularly, the ARMA type models were not useful)

Stochastic simulation strategy

- ◆ Stage 1: Generate annual time series
 - Use a parsimonious model yet capable of describing over-annual scaling
 - No need to describe sub-annual periodicity
- ◆ Stage 2: Disaggregate the annual into sub-annual time series
 - Use a parsimonious model structure such as PAR(1)
 - Couple it to the annual model
 - So, no need to describe over-annual scaling explicitly
- ◆ A one stage procedure to handle over-annual and sub-annual properties simultaneously has also been studied but not implemented operationally so far

Annual model: The generalized autocovariance function (GAS)

◆ General GAS expression

$$\gamma_j = \gamma_0 (1 + \kappa \beta |j|^\alpha)^{-1/\beta}$$

where γ_j : lag j autocovariance;
 γ_0 : variance; κ, α, β : parameters

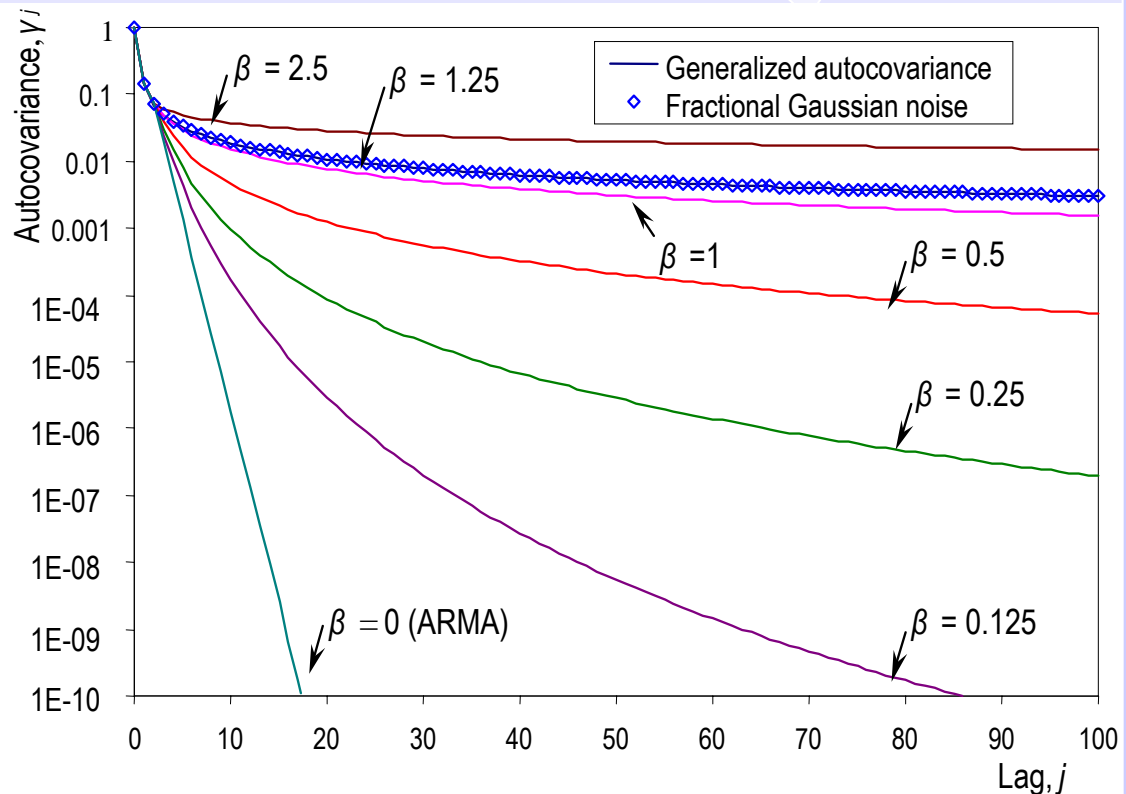
◆ Fittings options

- Optimize parameters to best fit historic autocorrelograms
- Preserve explicitly γ_1, γ_2 and Hurst exponent
- Explicit preservation of more γ_i is also possible

◆ GAS behavior

- For $\beta = 0 \Rightarrow$ ARMA:
 $\gamma_j = \gamma_0 \exp(-\kappa |j|^\alpha)$
- For $\kappa = (1/\beta) (1 - 1/\beta)^{-\beta}$
 $(1 - 1/2\beta)^{-\beta}$ and $\alpha = 1 \Rightarrow$
 FGN

Demonstration of GAS for $\alpha = 1$ and several values of β



Annual model: Generalized generating scheme for any covariance structure

Typical (backward) moving average (**BMA**) scheme: $X_i = \dots + a_1 V_{i-1} + a_0 V_i$
 where V_i independent random variables and a_i numerical coefficients

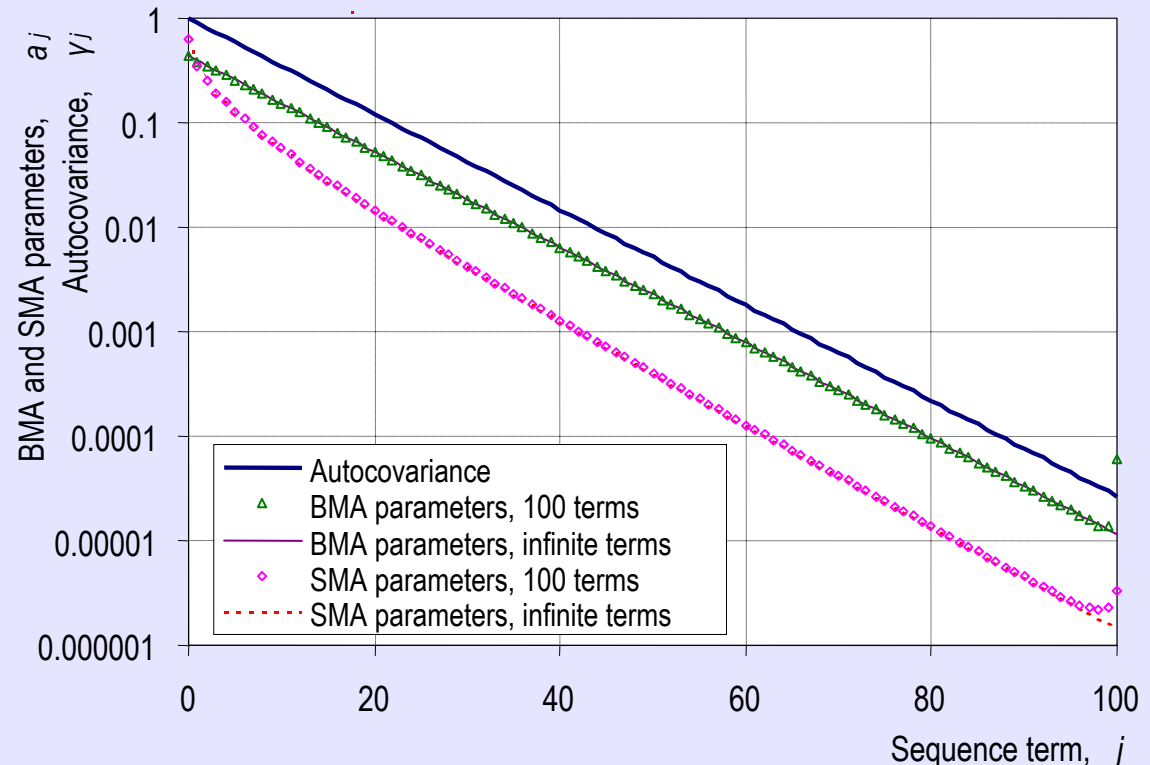
Symmetric moving average (**SMA**) scheme $X_i = \dots + a_1 V_{i-1} + a_0 V_i + a_1 V_{i+1} + \dots$

SMA has several advantages over BMA. Among them, it allows a closed solution for a_j :

$$s_a(\omega) = [2 s_y(\omega)]^{1/2}$$

where $s_a(\omega)$ and $s_y(\omega)$ the Discrete Fourier Transforms of the series a_j and y_j , respectively.

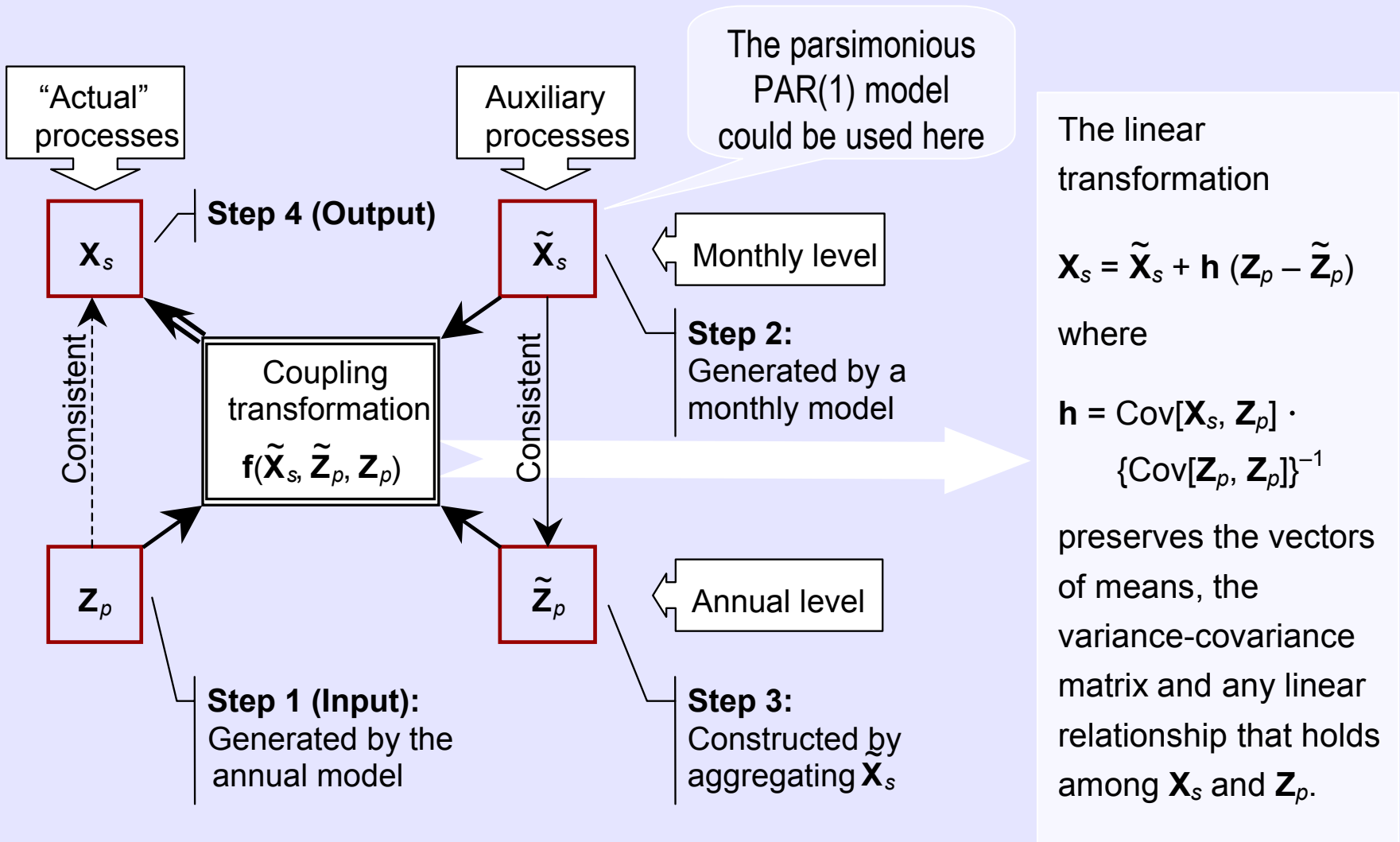
Both schemes are applicable for multivariate problems



Annual model: Stochastic simulation in forecast mode

- ◆ In forecast mode, the observed present and past values must condition the hydrologic time series of the future
- ◆ This is attainable using a two-step algorithm
 1. Generate future time series without reference to the known present and past values
 2. Adjust future time series using the known present and past values and a linear adjusting algorithm
- ◆ The linear adjusting algorithm:
 1. is expressed in terms of covariances among variables
 2. preserves exactly means, variances and covariances
 3. is easily implemented

Coupling stochastic models of different time scales



Handling of skewness in multivariate problems: Optimized decomposition of covariance matrices

- ◆ Consider any linear multivariate stochastic model of the form

$$\mathbf{Y} = \mathbf{a} \mathbf{Z} + \mathbf{b} \mathbf{V}$$

where \mathbf{Y} : vector of variables to be generated, \mathbf{Z} : vector of variables with known values, \mathbf{V} : vector of innovations, and \mathbf{a} and \mathbf{b} : matrices of parameters

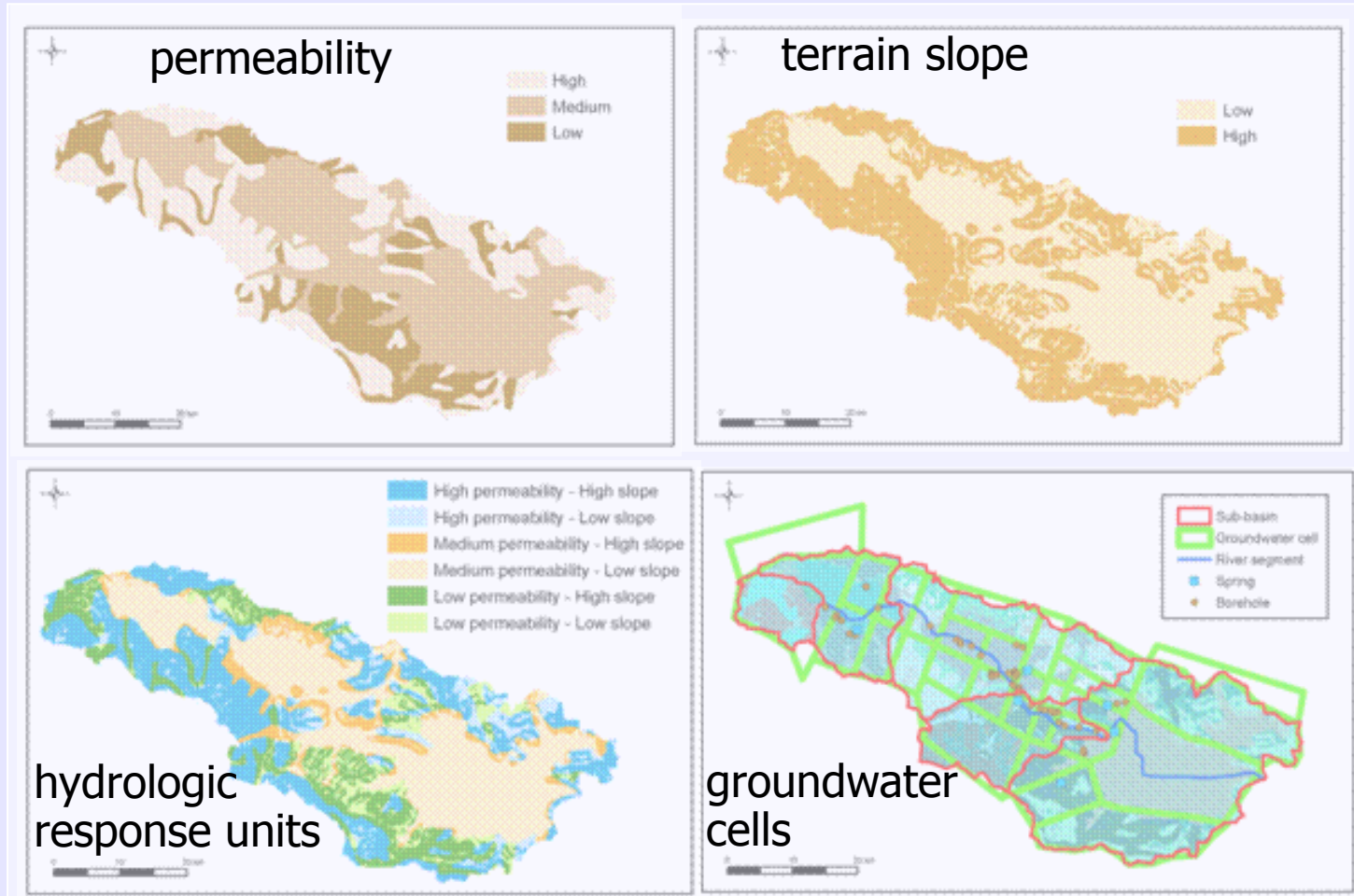
- ◆ The parameter matrix \mathbf{b} is related to a covariance matrix \mathbf{c} by

$$\mathbf{b} \mathbf{b}^T = \mathbf{c}$$

- ◆ This equation may have infinite solutions or no solution (if \mathbf{c} is not positive definite)
- ◆ The skewness coefficients ξ of innovations \mathbf{V} depend on \mathbf{b}
- ◆ The smaller the values of ξ , the more attainable the preservation of the skewness coefficients of the actual variables \mathbf{Y}
- ◆ Therefore, the problem of determination of \mathbf{b} can be seen as an optimization problem that combines
 - minimization of skewness ξ , and
 - minimization of the error $\|\mathbf{b} \mathbf{b}^T - \mathbf{c}\|$
- ◆ A fast optimisation algorithm has been developed for this problem
- ◆ The algorithm works even for \mathbf{c} that are not positive definite

Models developed are not only stochastic ...

In the Boeotikos Kephisos River basin a hydrologic model of the entire hydrologic cycle had to be developed, which was demanding due to the extended karstic activity and the intensive withdrawals for irrigation



3. Hydrosystem operation issues

Parameterization – Simulation – Optimization

Typical problems to be answered

- ◆ Find the **maximum possible annual release** from the system:
 - for a certain (acceptable) **reliability level** (steady state conditions)
 - for a certain **combination of the system components** (e.g. primary resources)and determine the corresponding:
 - **optimal operation policy** (storage allocation; conveyance allocation; pumping operation)
 - **cost** (in terms of energy; economy; other impacts)
- ◆ Find the **minimum total cost**
 - for a given **water demand** (less than the maximum possible annual release)
 - for a certain (acceptable) **reliability level**and determine the corresponding:
 - **combination of the system components** to be enabled
 - **optimal operation policy** (storage allocation; conveyance allocation; pumping operation)
 - **alternative operation policies** (that can satisfy the demand but with higher cost)

Categories of problems

- ◆ Steady state problems for the current hydrosystem
 - (e.g., previous slide)
- ◆ Problems involving time
 - Availability of water resources in the months to come
 - Impact of a management practice to the future availability of water resources
 - Evolution of the operation policy for a temporally varying demand
- ◆ Investigation of scenarios
 - Hydrosystem structure: Impacts of new components (aqueducts, pumping stations etc.)
 - Demand: Feasibility of expansion of domain
 - Hydroclimatic inputs: Climate change
- ◆ Adequacy/safety under exceptional events – Required measures
 - Damages
 - Special demand occasions (e.g. 2004 Olympic Games)

The methodology: General aspects

Question 1: Simulation **or** optimization?

- Simulation **versus** optimization (water resources literature and practice)
- Simulation methods **for** optimization (more mathematical literature)

Answer: Optimization coupled with simulation

Main advantages

- Determination of optimal policies
- Incorporation of mathematical optimization techniques

Main advantages

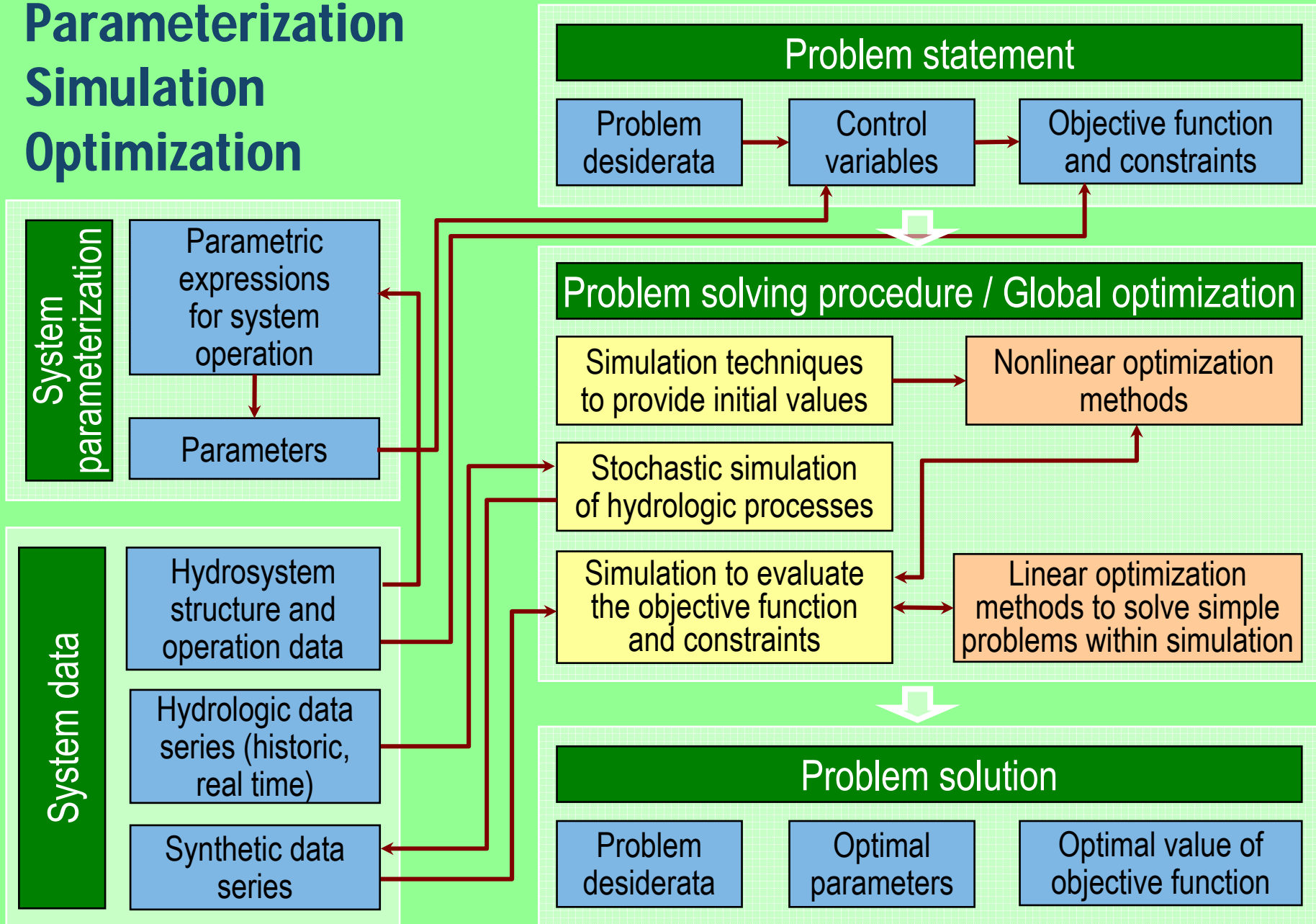
- Detailed and faithful system representation
- Better understanding of the system operation
- Incorporation of stochastic models

Question 2: Which are the control (decision) variables?

- Typically: Releases from system components in each time step

Answer: Introduction of **parametric control rules** with few **parameters** as control variables

Parameterization Simulation Optimization



Introduction to the parametric reservoir operation rule – Some analytical solutions

Maximize release from a simple reservoir system with single water use

◆ Case a: no conveyance restrictions; no leakages

- Solution: Probability of spill equal at all reservoirs (**New York Rule**; Clark, 1950)
- Under certain (rather common) conditions about the distribution of inflows:

Space rule

(Bower et al., 1962)

$$\frac{K_i - S_i}{E[CQ_i]} = \frac{\sum K - V}{\sum E[CQ]}$$

◆ Case b: no conveyance restrictions; significant leakages; insignificant spills

- Solution:

Leakage rule (Nalbantis & Koutsoyiannis, 1997)

$$S_i = \begin{cases} V & \text{for one reservoir} \\ 0 & \text{for all others} \end{cases}$$

◆ Case c: restricted conveyance capacity; insignificant spills; no leakages

- Solution:

Conveyance rule (Nalbantis & Koutsoyiannis, 1997)

$$\frac{S_i}{C_i} = \frac{V}{\sum C}$$

Notation: i = Reservoir index, K = Storage capacity, S = Storage, $V = \sum S$, CQ = Cumulative inflow, $E[\]$ = expectation, C = Conveyance capacity

Formulation of the parametric reservoir operation rule

Initial linear parametric form

$$S_i^* = a_i + b_i V \quad (\text{parameters } a_i, b_i)$$

subject to $\sum a_i = 0, \sum b_i = 1,$

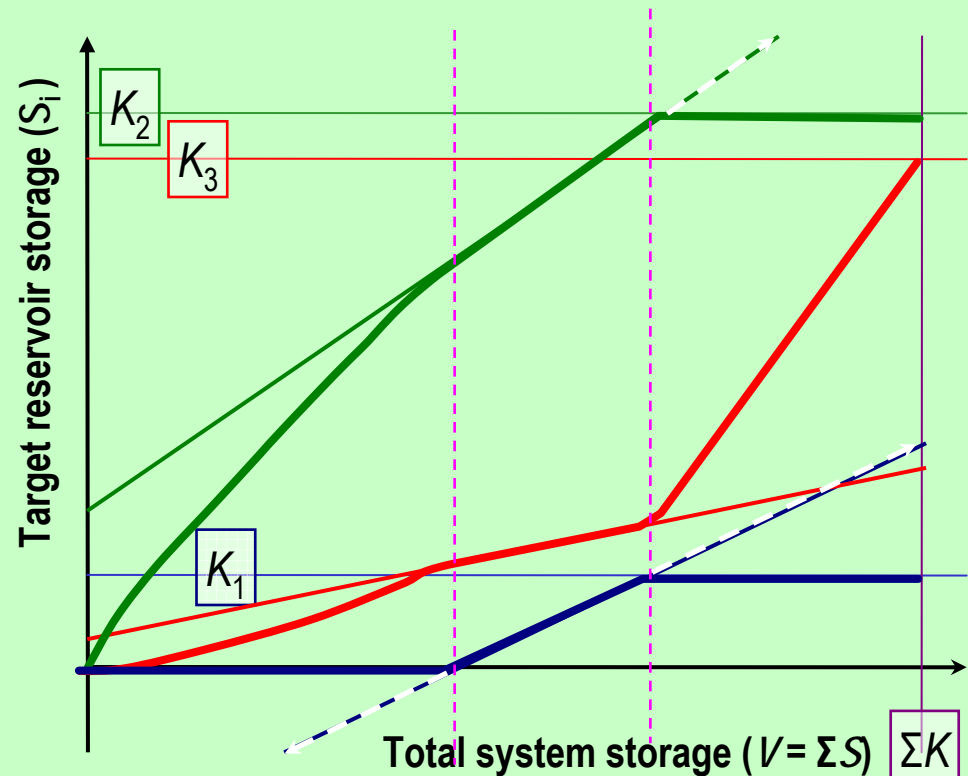
since $\sum S_i^* = V$

Corrected for physical constraints

$$S_i^{**} = \begin{cases} 0 & a_i + b_i V < 0 \\ a_i + b_i V & 0 \leq a_i + b_i V \leq K_i \\ K_i & a_i + b_i V > K_i \end{cases}$$

Adjusted, nonlinear form

$$S_i^{***} = S_i^{**} + \frac{S_i^{**}(1 - S_i^{**}/K_i)}{\sum S_j^{**}(1 - S_j^{**}/K_j)} (V - \sum S_j^{**})$$



Two parameters per reservoir (a_i, b_i) = **Control variables**

Parameter values **determined by optimization** – depending on the objective function

Parameters may depend also on season (e.g., refilling-emptying period, or months)

$2 \times (\text{reservoirs} - 1) \times \text{seasons}$ total parameters for the reservoir system

A comparison with non-parametric optimization

Problem: Find the maximum release that can be ensured by a system of **3 reservoirs** with **reliability 99%** (probability of failure 1%). Use **1000 years** of simulated data with **monthly time step**. Assume **steady state** conditions.

Non-parametric optimization

Number of control variables:

$$\begin{aligned} & 1000 \times 12 \text{ monthly releases} \\ & \times (3 - 1) \text{ reservoirs} + 1 \text{ (problem target)} \\ & = 24001 \end{aligned}$$

Cannot be combined with simulation

All physical constraints of the system must be entered as problem constraints

Control variables depend on inflow series

Implicit assumption of known inflows (perfect foresight)

The optimization model needs continuous runs with updated data

Parametric rule based optimization

Number of control variables:

$$\begin{aligned} & 2 \text{ parameters/reservoir/ season} \\ & \times (3 - 1) \text{ reservoirs} \times 2 \text{ seasons} \\ & + 1 \text{ (problem target)} \\ & = 9 \text{ (as an order of magnitude)} \end{aligned}$$

Can be combined with simulation

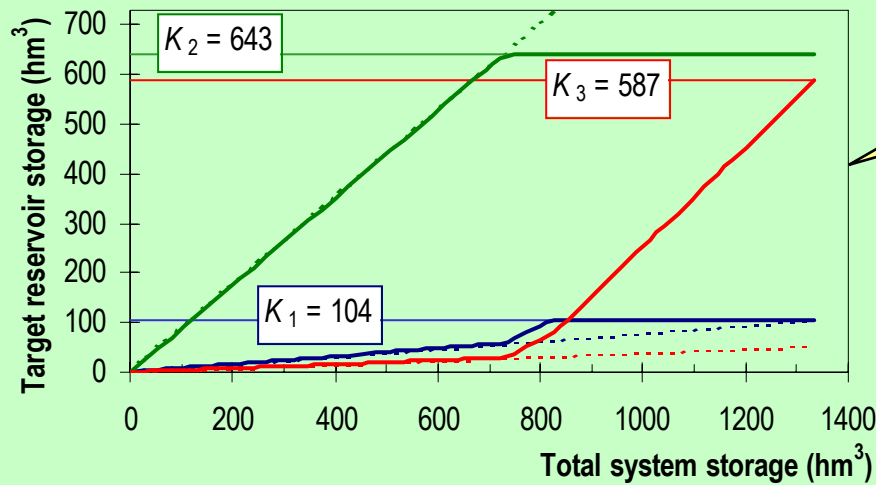
Physical constraints of the system are handled by the simulation model

Control variables do not depend on inflow series but on their statistical properties

No assumption of known inflows

Once parameters are optimized, the system can be operated without running the model

Application of the parametric rule – Optimal results



Maximization of system release

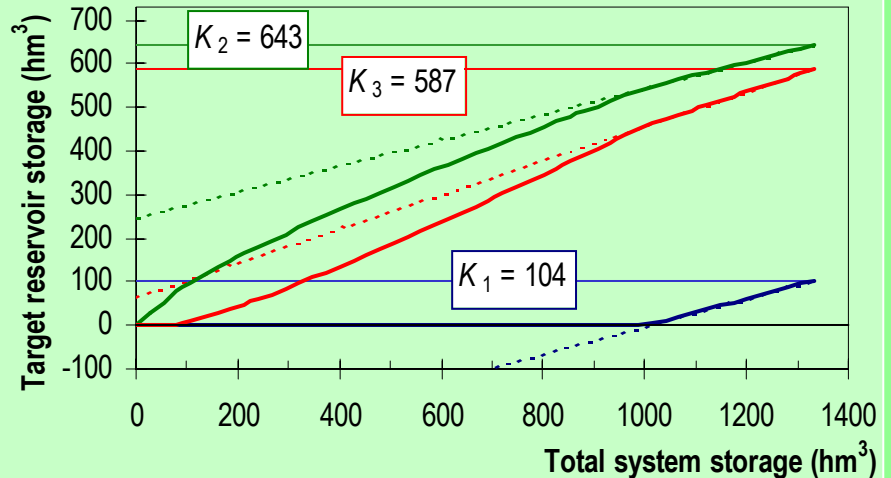
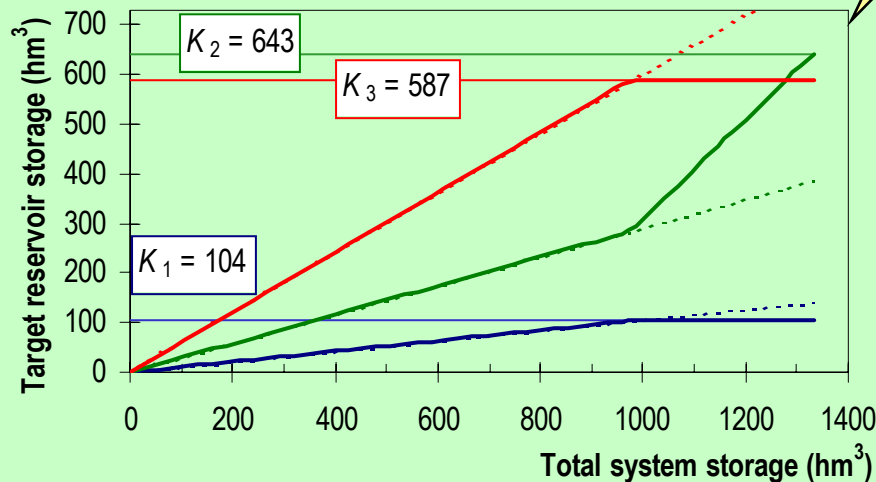
— Evinos

— Mornos

— Hylke

Minimization of cost for system release = 87% of maximum

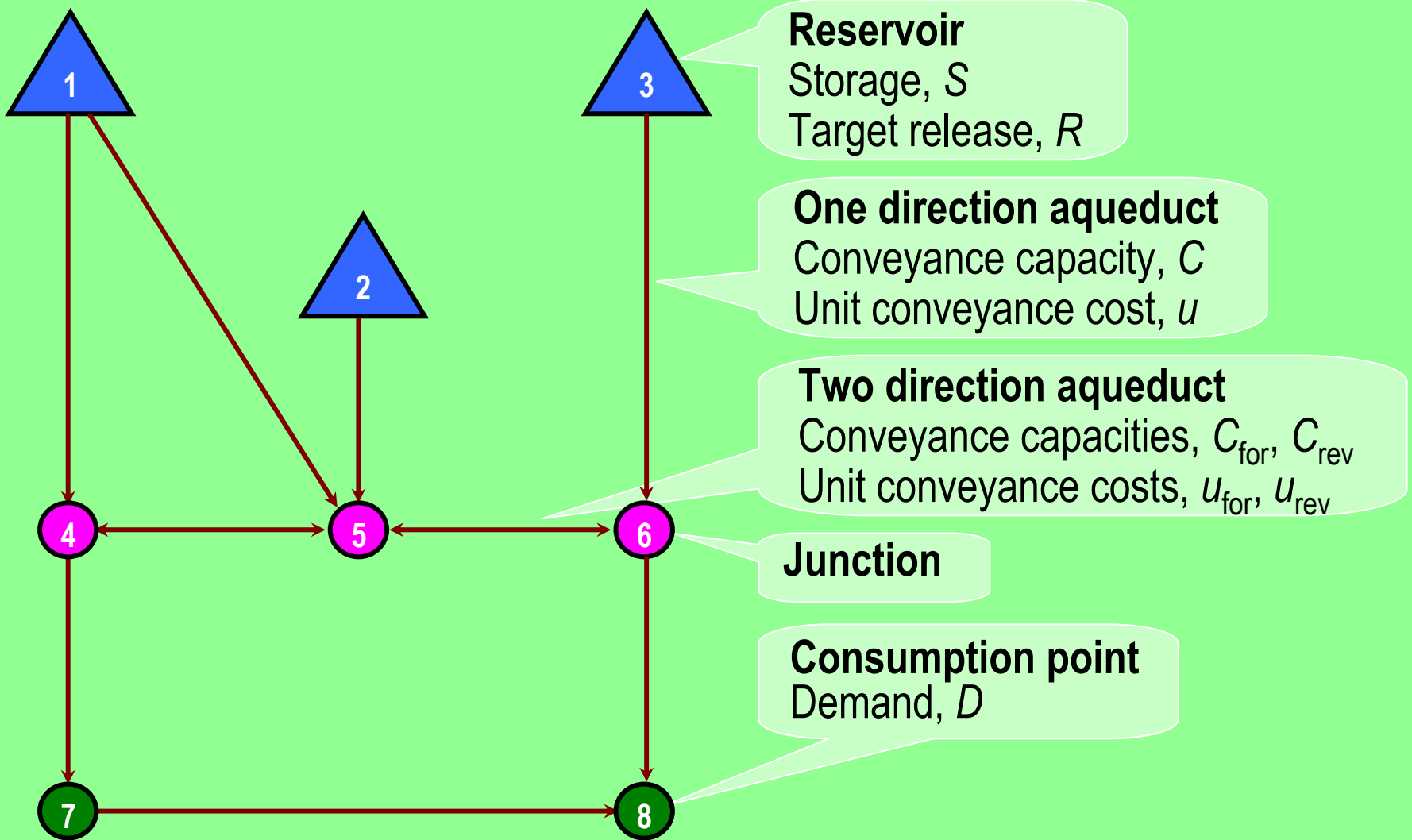
Maximization of system release but with no leakage at Hylke



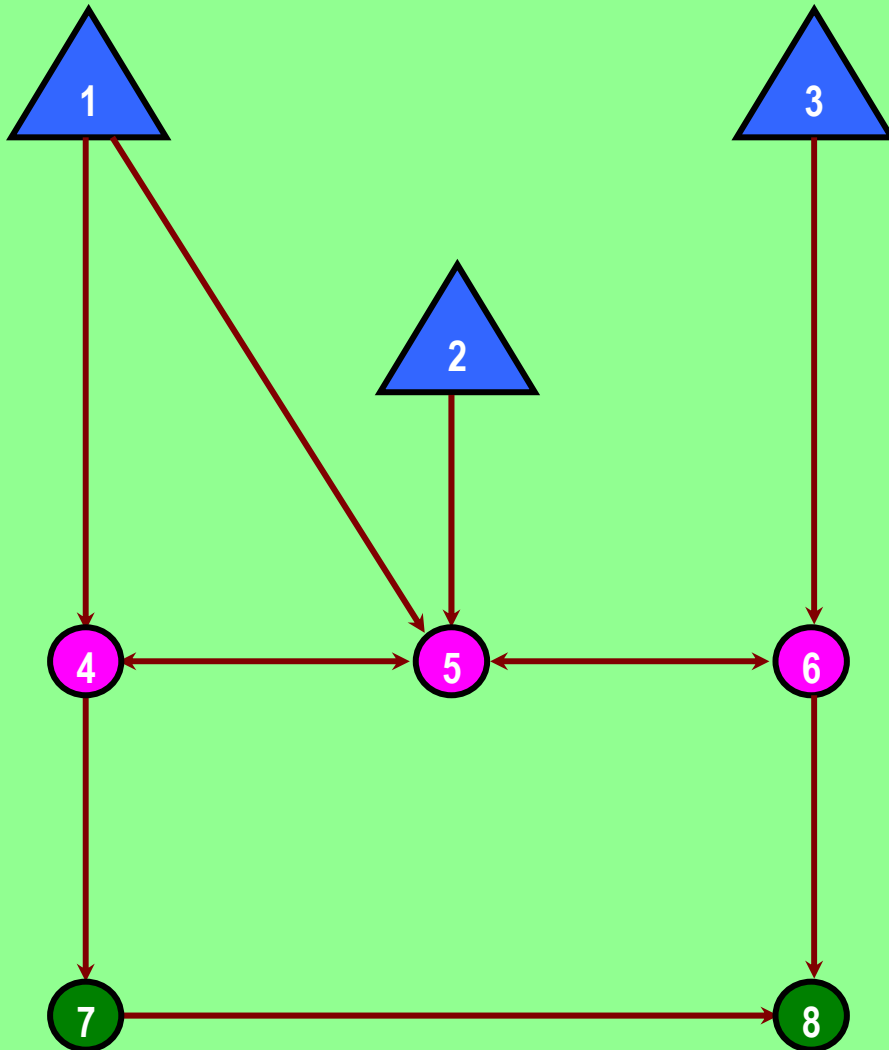
Considering the complete hydrosystem – Simulation

- ◆ Assuming that parameters a_i and b_i are known, the **target releases** from each reservoir will be also known in the beginning of each simulation time step
- ◆ The **actual releases** depend on several attributes of the hydrosystem (physical constraints)
- ◆ Their estimation is done using **simulation**
- ◆ Within simulation, an **internal optimization** procedure may be necessary (typically linear, nonparametric)
- ◆ Because parameters a_i and b_i are not known, but rather are to be optimized, simulation is driven by an **external optimization** procedure (nonlinear)

Hydrosystem components and attributes



Conveyance problem formulation



Given:

- Demands (D)
- Reservoir storages (S),
- Reservoir target releases ($R \leq S$; $\sum R = \sum D$; from parametric rule)

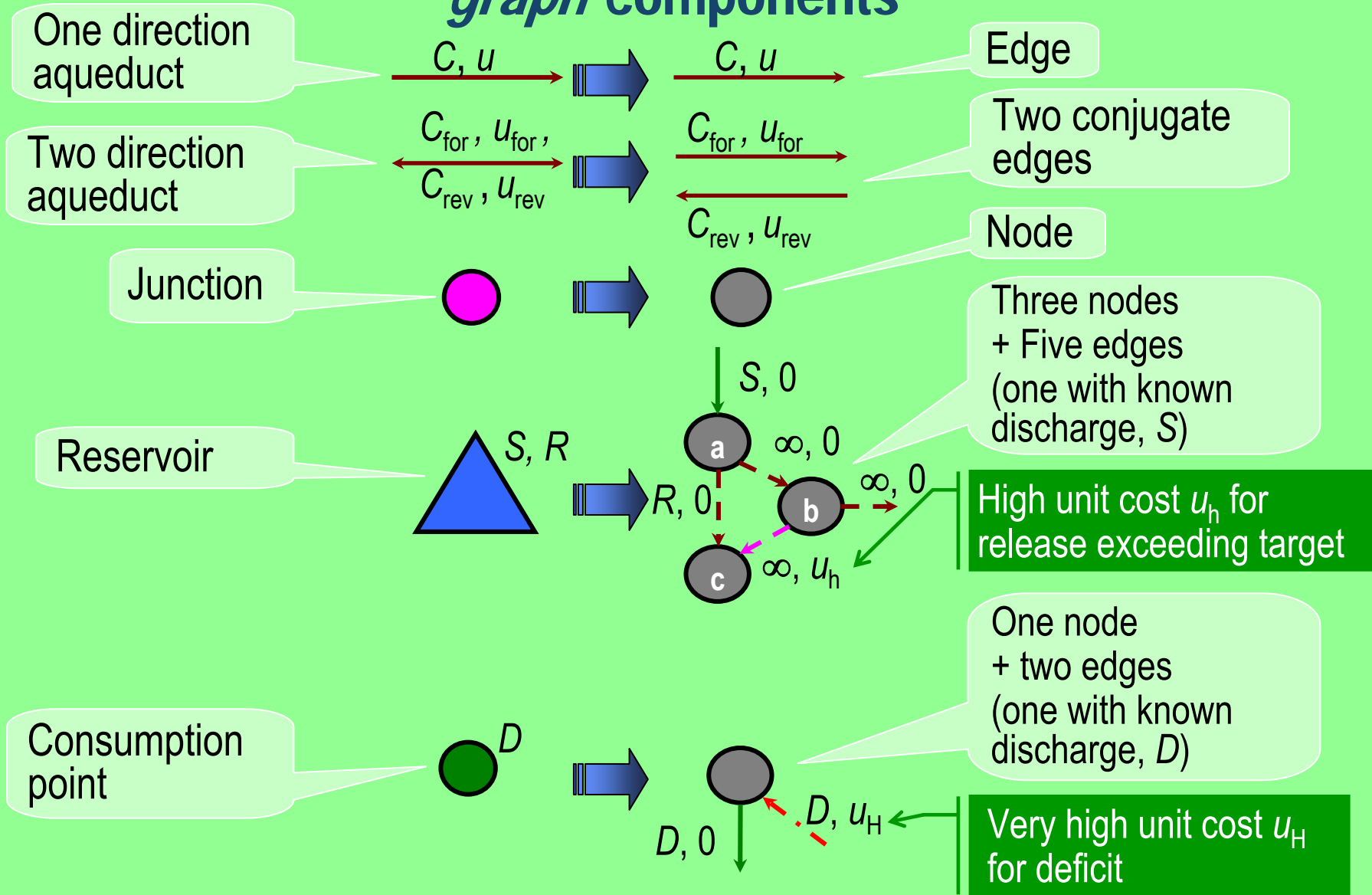
Required:

- Actual (feasible) consumptions (at consumption points)
- Actual (feasible) releases (from reservoirs)
- Aqueduct discharges
- Conveyance cost

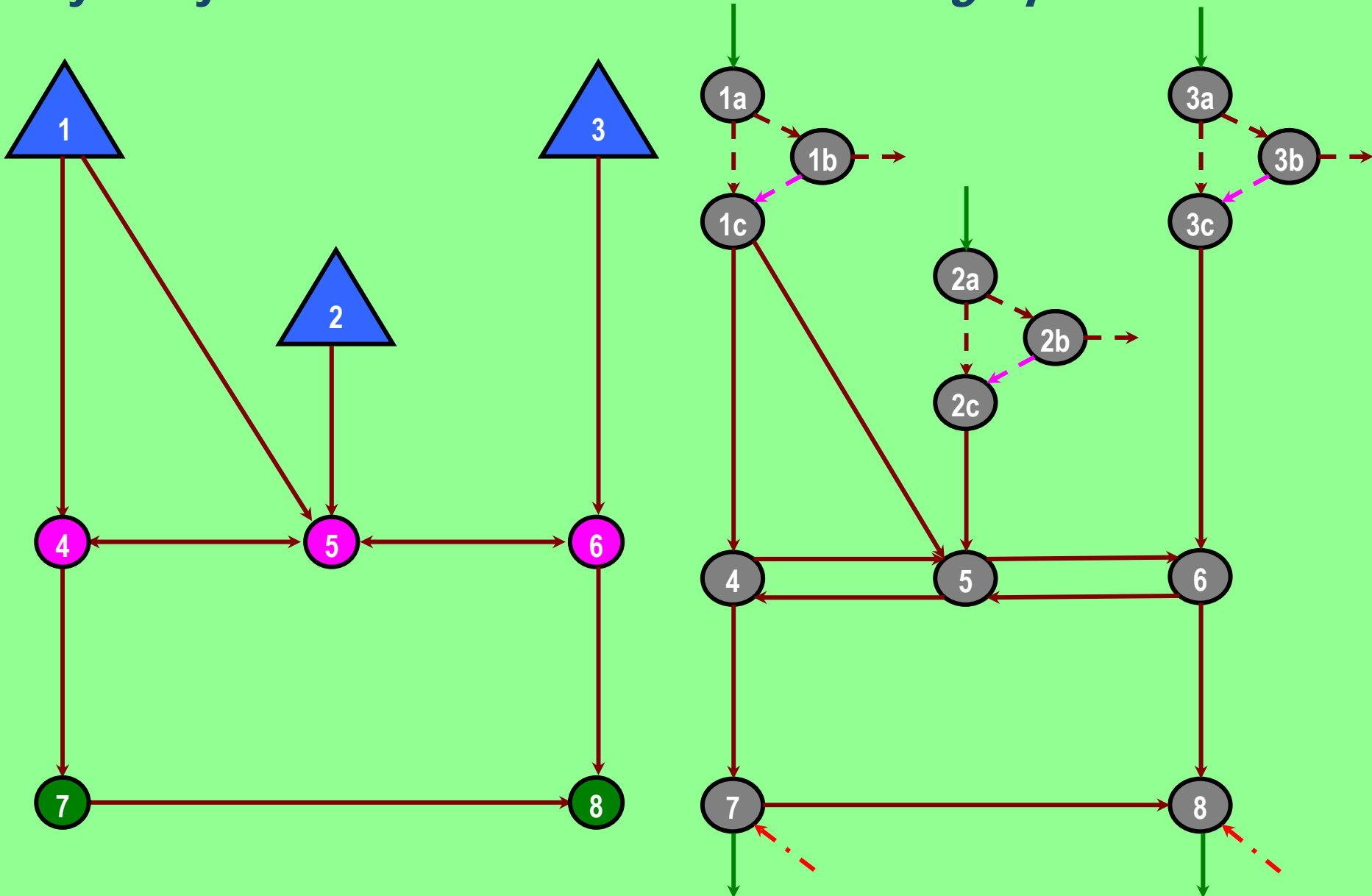
Conditions:

- If possible, no deficits at consumption points
- If possible, releases from reservoirs equal to target releases
- Minimum conveyance cost

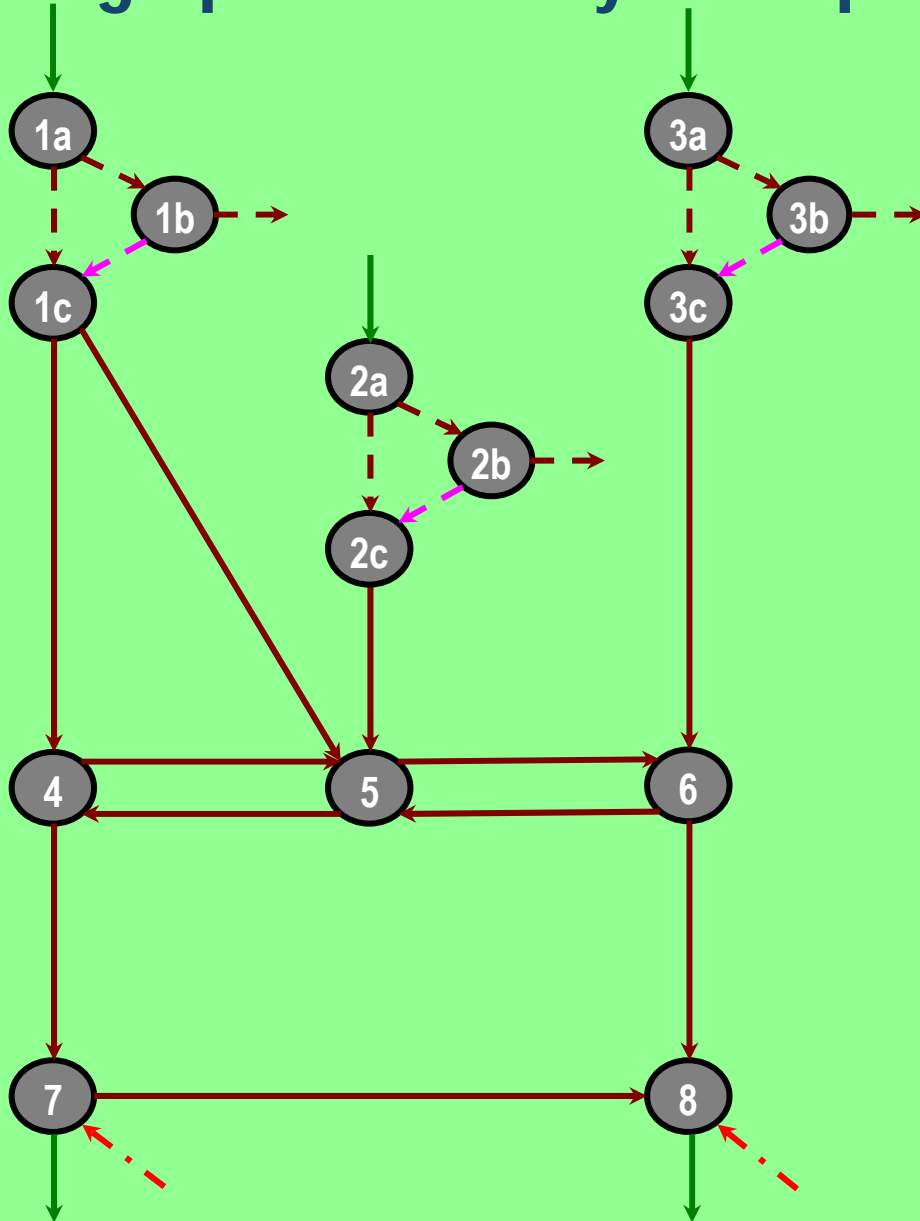
Transformations of hydrosystem components to *graph* components



Hydrosystem and its transformation to *digraph*



Digraph solution by linear programming



Determine all unknown discharges Q_{ij} at edges ij , by **minimizing total cost**

$$TC = \sum_{ij} u_{ij} Q_{ij}$$

subject to equality constraints for each node i

$$\sum_j Q_{ij} - \sum_j Q_{ji} = 0$$

and to **inequality constraints** for each edge ij

$$0 \leq Q_{ij} \leq C_{ij}$$

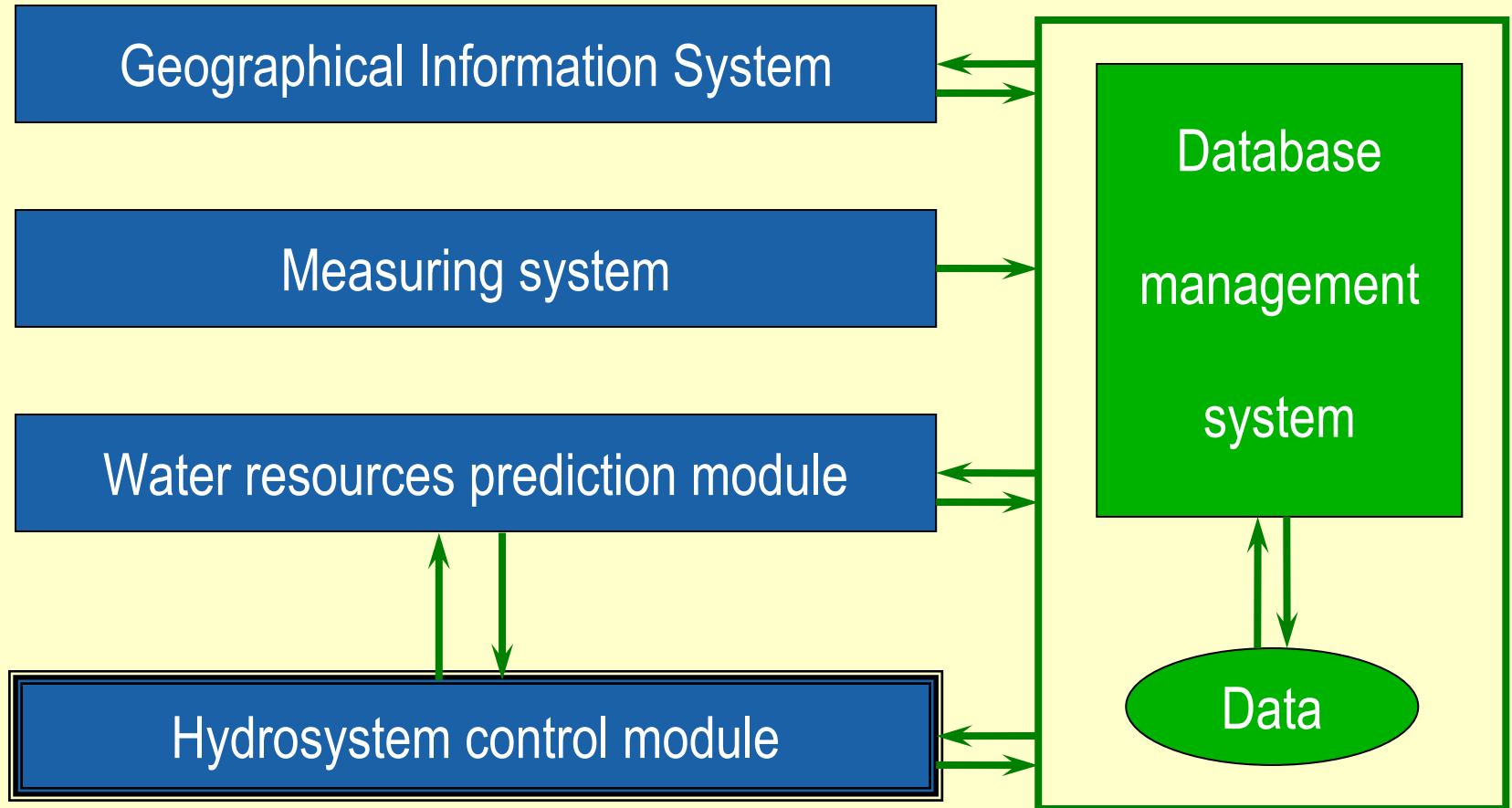
General evaluation and extensions of the parameterization-simulation-optimization method

- ◆ Is parametric rule underparametrized?
 - Nonlinear expressions with three parameters per reservoir did not outperform
 - Homogeneous linear expressions (one parameter per reservoir, $a_i = 0$) result in almost same optimal solutions
 - Considering seasonality (2 seasons) may improve results (slightly)
- ◆ How results of parametric rule based optimization compare to those of nonparametric optimization methods?
 - Generally, they are not inferior
 - In the non realistic case of *perfect foresight*, high dimensional methods may outperform parametric method *with no foresight* (slightly, by about 2%)
 - In practice, in complex nonlinear problems the parametric method yields better solutions due to more effective locating of global optimum
- ◆ Is the parameterization appropriate for all water uses and hydrosystems?
 - Yes, but different parameterizations may be needed for different components (e.g. aquifers)
 - Successful application to hydropower systems

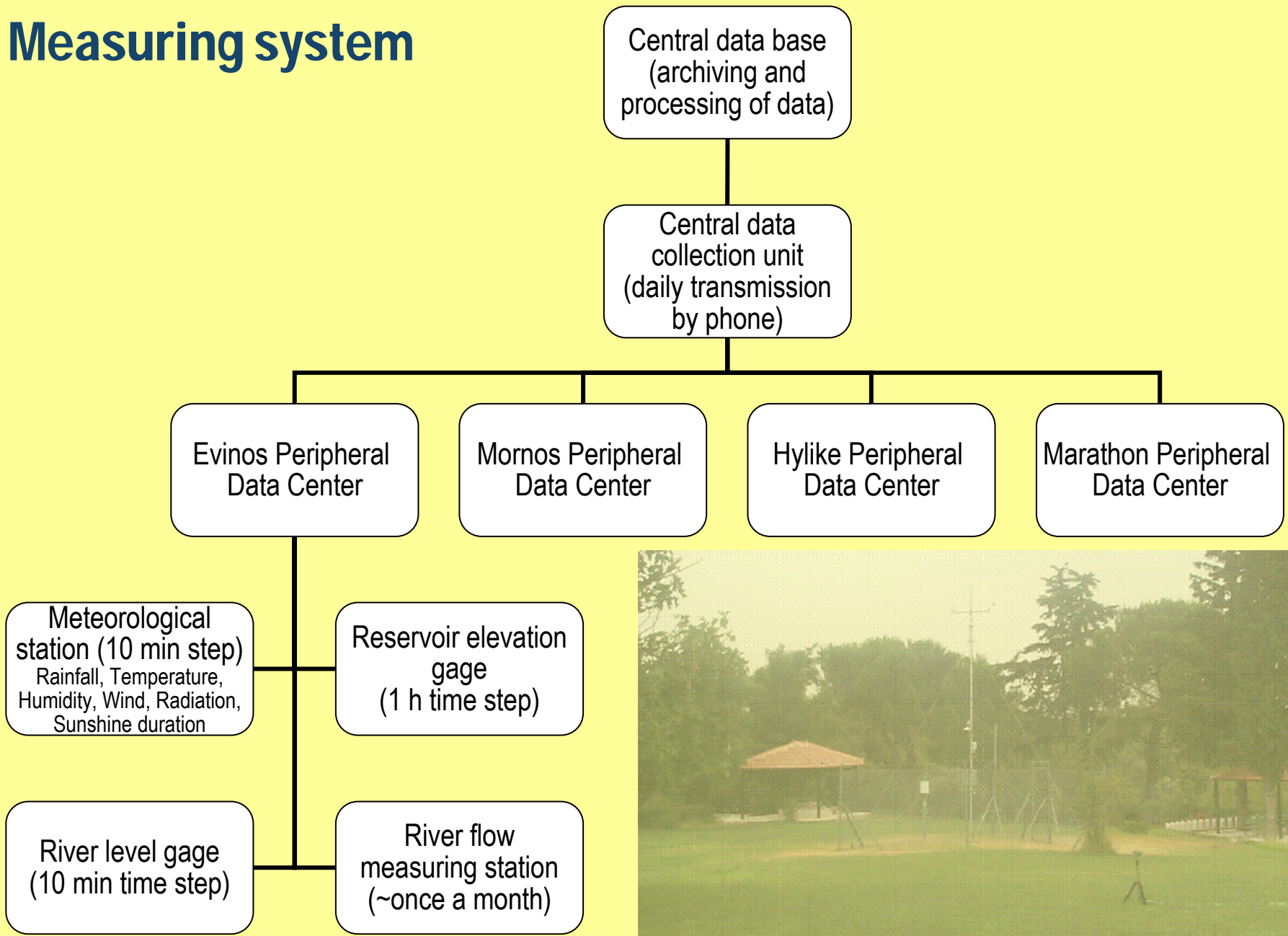
Decision support tool integration

Data acquisition – Software systems – Management plans

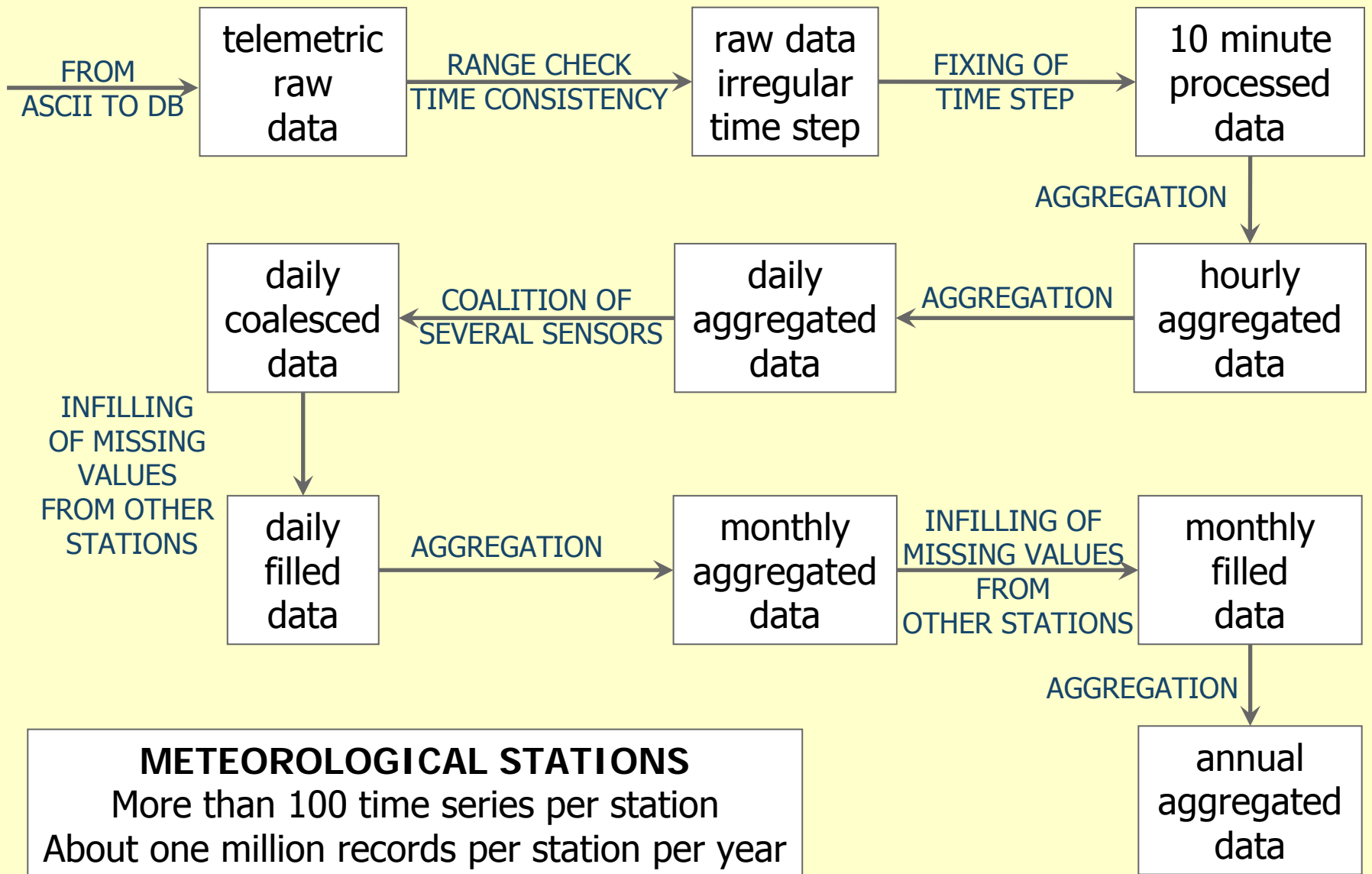
Decision support tool structure



Measuring system



Data management and processing: Time series manipulation



Software system characteristics

- ◆ All models written from scratch
- ◆ Basic development tool: **Delphi** (Object Pascal)
- ◆ Database: **Oracle** (more recently: **PostgreSQL**)
- ◆ Geographic system: **ArcView**
- ◆ Basic software units
 - **Hydrognomon**: Database management, processing of hydrologic data
 - **Castalia**: Stochastic hydrologic simulator
 - **Hydrogeios**: Simulation of surface and ground water processes
 - **Hydronomeas**: Hydrosystem control

Hydrognomon: Processing of hydrologic time series

The screenshot displays the Hydrognomon software interface, which is used for processing hydrologic time series. The main window shows a time series graph with a menu bar (File, Edit, View, Help) and a toolbar. The graph plots Stage (m) on the Y-axis against time from 1968 to 1970. Below the graph is a data table with columns for year and stage values.

The 'Interpolations (Stage-Discharge)' dialog box is open, showing the following options:

- Type of Calculations:
 - Stage-Discharge
 - Stage-Area, Volume
 - Stage-Leakage
 - Spillway Stage-Discharge
- Load Curves: from File, from DB
- Save Curves: to File, to DB
- Required Time Series:
 - Dense Stage TS (Required)
 - Sparse Stage TS (Accurate)
 - H-Q measurements, Stage TS
 - H-Q measurements, Discharge
- Assign to: (Double Click to change)
 - 61 ()
 - 60 ()
- Options:
 - Make H1 Correction (from Accu...)
 - Merge Sparse + Dense Stage Data
 - Make H2 Correction (from H-Q)
 - Make Stout Correction
 - Calculate Discharge

The 'Statistics' dialog box is also open, showing a list of distribution curves and a 'Calculate' button. The 'Distribution curves' list includes:

- Normal (Gauss)
- Log Normal
- Galton (Log 3p)
- Exponential
- Gamma (2p)
- Pearson III (G 3p)
- Log Pearson III
- EV-1Max (Gumbel)
- EV-2Max
- EV-1Min (Gumbel)
- EV-3Max (Gumbel)
- GEV-Max
- GEV-Min
- Pareto
- GEV-Max (K spc.)
- GEV-Min (K spc.)
- L-Moments

The 'Calculate' button is highlighted, and the 'Calculate' dialog box is open, showing a list of calculations to perform:

- Calculate instantaneous values
- Calculate inst., monthly & yearly cumulative values
- Calculate inst., monthly & yearly averages

The main graph shows a log-log plot of Stage (m) versus Discharge (m³/s). The Y-axis ranges from 0 to 10, and the X-axis ranges from 0.1 to 1,000. The plot shows data points for various time periods, with a fitted curve and confidence intervals. The legend indicates the following time periods:

- 1/1/1992 - 11/12/1995
- 12/1/1995 - 13/1/1997
- 14/1/1997 - 16/1/1999
- 12/1/1999 - 31/12/2000
- 1/1/1992 - 31/12/2000 (Ext.)

The 'Probability function (%) - scale: Normal distribution' plot shows the distribution of discharge values, with a scale from 0.05% to 99.9%.

At the bottom of the interface, there is a text box with the instruction: "Drag with left mouse button from left to bottom right to zoom, drag with right button to move the graph (pan)".

Hydrognomon: Automatic lumped hydrologic modeling

The image displays the Hydrognomon software interface for Basin Simulation. The main window is titled "Basin Simulation" and includes a menu bar (File, Edit) and tabs for Simulation, Calibration, and Dates. The interface is divided into several sections:

- Simulation Settings:** Includes checkboxes for "Potential Evapotranspiration" and "Pumping". Below these are lists for parameter selection (0: Βροχόπτωση, 1: Εξάτμ., 2: Αντήληση, 3: Απορροή) and input fields for "K: Soil Storage Capacity (mm)" (500) and "Initial Soil Storage (S0, mm)" (0). A "Percolation" section includes a checkbox and a value of 0.50.
- Ground Tank Settings:** Includes a checkbox for "Pumping" and a list for parameter selection. Input fields for "Initial Ground Storage (Y0, mm)" (0) and "Base flow" (5 μ) are present. A "Calibrate" section shows "Preset / Calibrated Values" for parameters like κ (0.129), λ (0.000), ξ (0.047), and others.
- Graphical Representation:** A central area with a diagram showing the flow between the Soil Tank and Ground Tank. It includes a "Graphical Representation" section with a value of 0.50 and a "Measured runoff" checkbox.
- Output Timeseries:** A section with checkboxes for "Runoff", "Evapotranspiration", "Percolation", "Soil storage", "Ground storage", and "Error".
- Calibration Results:** A table of "Preset / Calibrated Values" for various parameters:

κ	λ	ξ	φ	K	H1/K	H2	S0/K	Y0
0.129	0.000	0.047	0.116	0.054	0.010	215.90	0.000	224.72
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	250.96
- Objective Function and Iterations:** Shows an "Objective Function" value of 0.848 and "Number of Iterations" of 8000. Buttons for "Calibrate", "Transfer from model", and "Transfer to model" are available.
- Graph:** A line graph at the bottom showing "Actual Runoff" (red line) and "Calcu. Runoff" (green line) over time from 1985 to 1993. The y-axis represents runoff volume (0 to 120).

Hydrogeios: Detailed geo-hydrologic modeling

Groundwater cells

General information

Name:

Description:

Properties

Type: Groundwater tank Bottom (m): 280.000

X - centroid (m): 372089 Porosity: 0.269

Water balance timeseries (level in m, else in m3)

Date	Storage	Percolation	Infiltration	Pumping	Sim. level	Real level
Οκτ-84	122461	25493	229360	0	280.010	0.000
Νοε-84	1036255	1748228	324905	0		
Δεκ-84	1514703	2364798	348420	0		
Ιαν-85	4888994	6175260	3418377	0		
Φεβ-85	4460661	4424469	1879408	0		
Μαρ-85	3583788	3570247	1908831	0		
Απρ-85	2604403	2297939	1622415	273386		
Μαϊ-85	1233929	1422955	610134	637346		
Ιουν-85	321721	827474	293403	1045847		
Ιουλ-85	274	464671	217745	1354580		

HydroGeios

Project Schematization Layers Hydrology Calibration Run Results Help

Calibrated model responses

Properties

Process type: River discharge

Model component: Σίρραγα Καρδίστας (4)

Discharge series (m3/s)

Date	Simulated	Observed
Οκτ-84	5.425	4.400
Νοε-84	7.145	7.700
Δεκ-84	6.938	10.200
Ιαν-85	33.719	38.600
Φεβ-85	24.190	18.500
Μαρ-85	22.341	24.500
Απρ-85	15.115	19.800
Μαϊ-85	4.261	6.600
Ιουν-85	0.000	2.800
Ιουλ-85	0.000	0.000
Αυγ-85	0.000	0.200
Σεπ-85	1.677	2.400
Οκτ-85	7.505	6.700
Νοε-85	9.371	10.200
Δεκ-85	12.012	11.600
Ιαν-86	12.889	10.300
Φεβ-86	19.231	16.700
Μαρ-86	14.858	15.700
Απρ-86	6.202	7.300
Μαϊ-86	2.678	3.800
Ιουν-86	0.000	0.800
Ιουλ-86	0.000	0.000

Statistics

Statistical measure	Calibration	Validation
Average of observed series	7.438	5.502
Average of simulated series	7.524	6.537
St. deviation of observed series	8.360	6.683
St. deviation of simulated series	7.961	8.076
Coef. of variation of observed series	1.124	1.215
Coef. of variation of simulated series	1.058	1.235

Performance measures

Performance measure	Calibration	Validation	Weight
Nash-Sutcliffe measure	0.887	0.751	8.000
Average bias	-0.012	-0.188	0.100
St. deviation bias	0.048	-0.208	0.100
Coef. of variation bias	0.059	-0.017	0.000
Intermittence flow error	1.066	0.999	1.000
Kendall variable	0.115	0.064	0.000
Value in obj. function	1.978	3.034	

Basins

General information

Name: Λεκάνη ανάντη άνω που

Description:

Properties

Area (km2): 106.200

Mean elevation (m): 957.900

Length of main tributary (km): 0.000

Average slope (%): 0.000

Downstream node: Γραβιά

Parent river section: No river assigned

Water balance timeseries (mm)

Date	Precipitation	Pot. evapor.	Real evapo	Percolation	Infiltration	Runoff	Soil storage	Evap. storag
Οκτ-84	6.3	63.0	5.9	0.1	0.0	0.1	0.3	0.0
Νοε-84	209.8	27.1	27.0	46.2	0.0	2.5	133.6	0.0
Δεκ-84	116.9	21.0	20.9	54.6	0.0	6.3	169.7	0.0
Ιαν-85	475.2	35.3	35.2	132.2	0.0	174.8	366.4	0.0
Φεβ-85	101.9	28.4	28.3	93.3	0.0	74.1	298.1	0.0
Μαρ-85	156.1	43.3	43.1	85.9	0.0	68.0	282.4	0.0
Απρ-85	109.9	91.4	91.1	60.3	0.0	44.6	217.6	0.0
Μαϊ-85	67.3	117.7	81.3	40.1	0.0	39.8	153.5	0.0
Ιουν-85	21.9	160.5	52.5	24.5	0.0	0.7	97.6	0.0
Ιουλ-85	17.7	173.5	39.1	14.4	0.0	0.2	61.6	0.0
Αυγ-85	0.0	168.2	15.0	8.4	0.0	0.0	38.2	0.0
Σεπ-85	24.9	102.5	27.9	5.7	0.0	0.3	29.1	0.0
Οκτ-85	143.9	49.2	49.0	28.1	0.0	1.7	93.6	0.0
Νοε-85	297.5	31.7	31.6	82.1	0.0	54.2	243.9	0.0
Δεκ-85	111.2	21.4	21.3	73.8	0.0	46.6	234.7	0.0
Ιαν-86	178.1	32.6	32.5	82.2	0.0	57.4	261.7	0.0
Φεβ-86	305.5	37.4	37.3	112.0	0.0	147.9	334.4	0.0
Μαρ-86	133.9	49.9	49.7	87.6	0.0	69.4	286.8	0.0

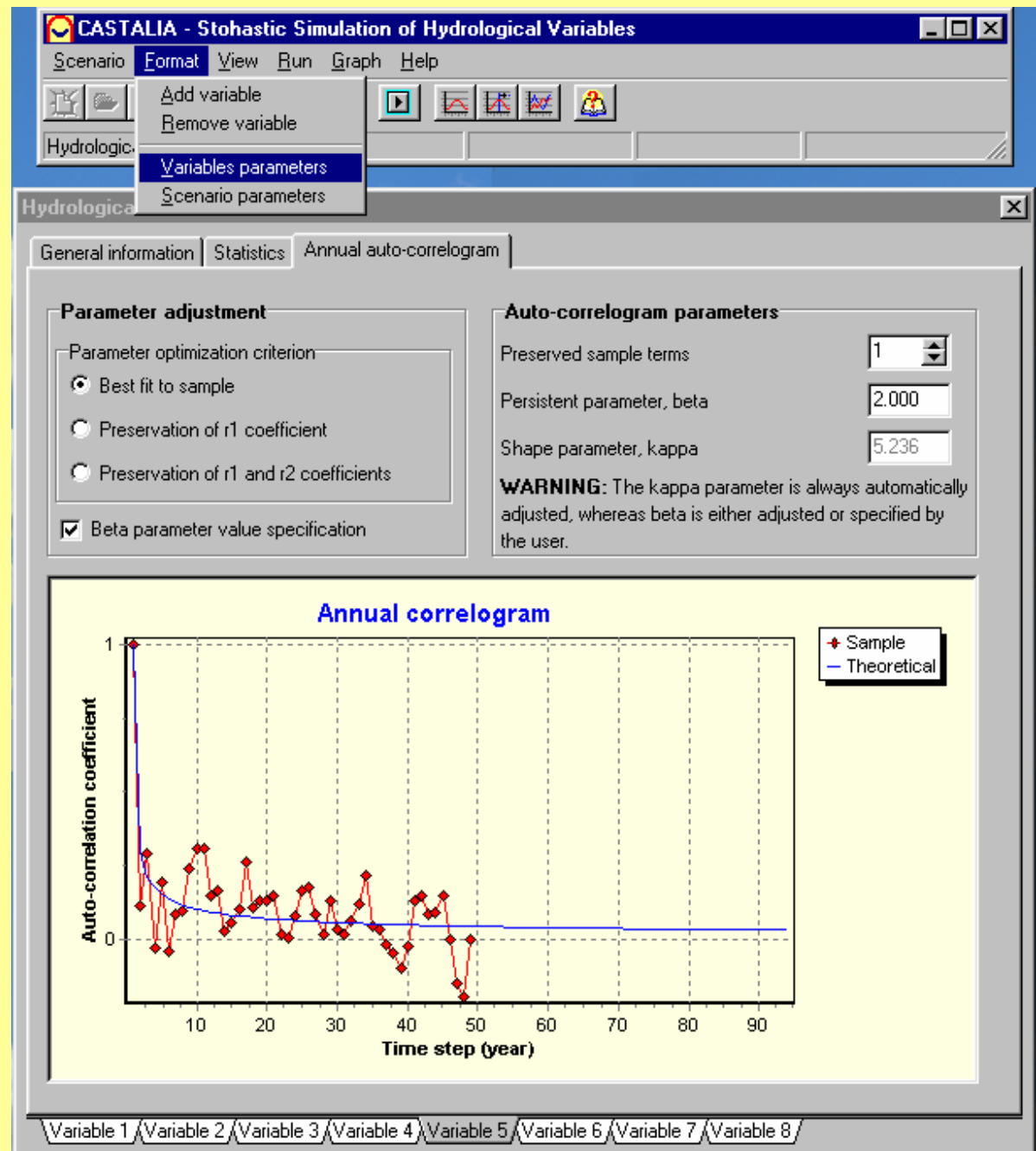
Precipitation

Basin 0 | Basin 1 | Basin 2 | Basin 3 | Basin 4

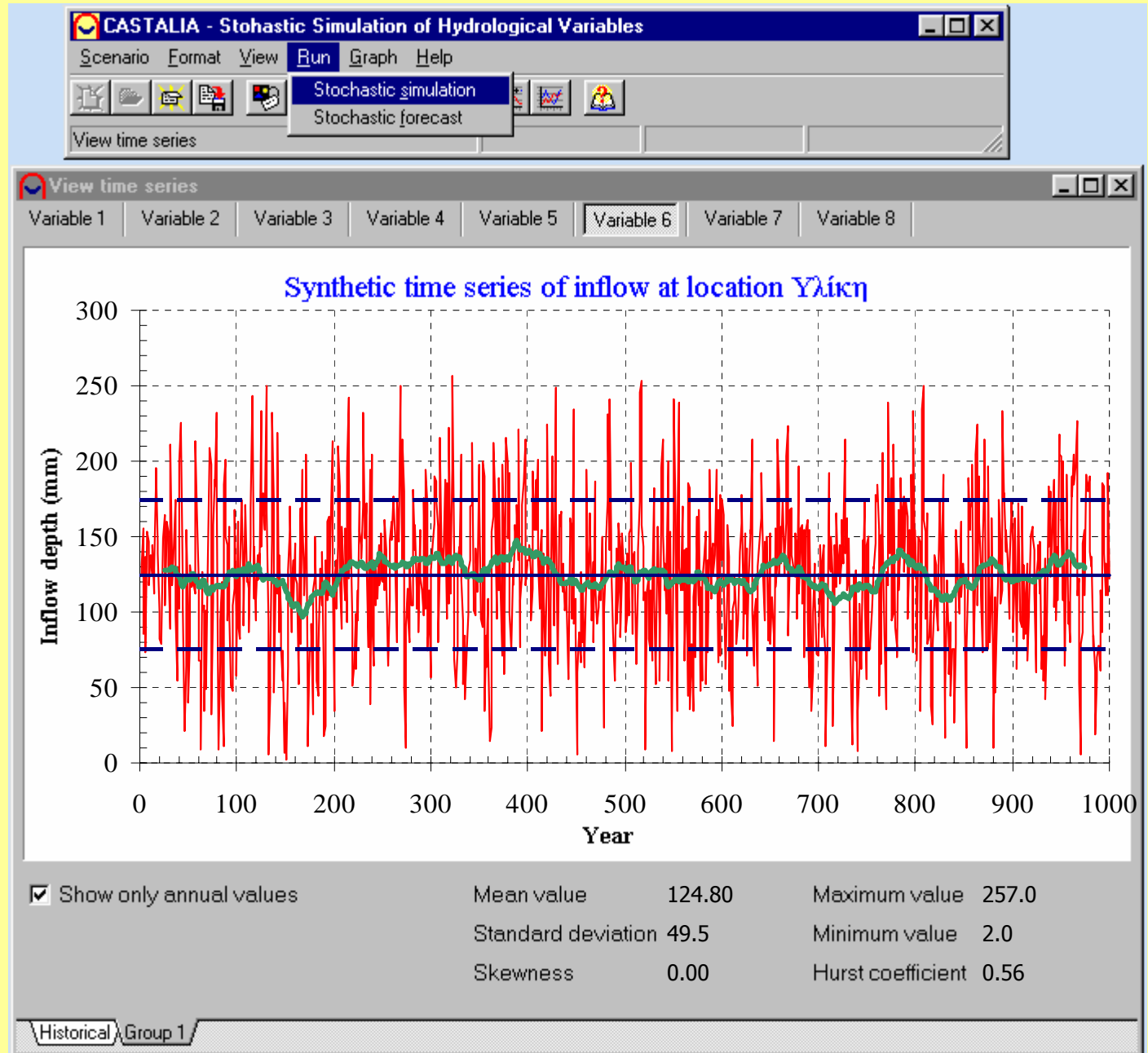
Discharge (m3/s)

Response 0 | Response 1 | Response 2 | Response 3 | Response 4 | Response 5 | Response 6 | Response 7

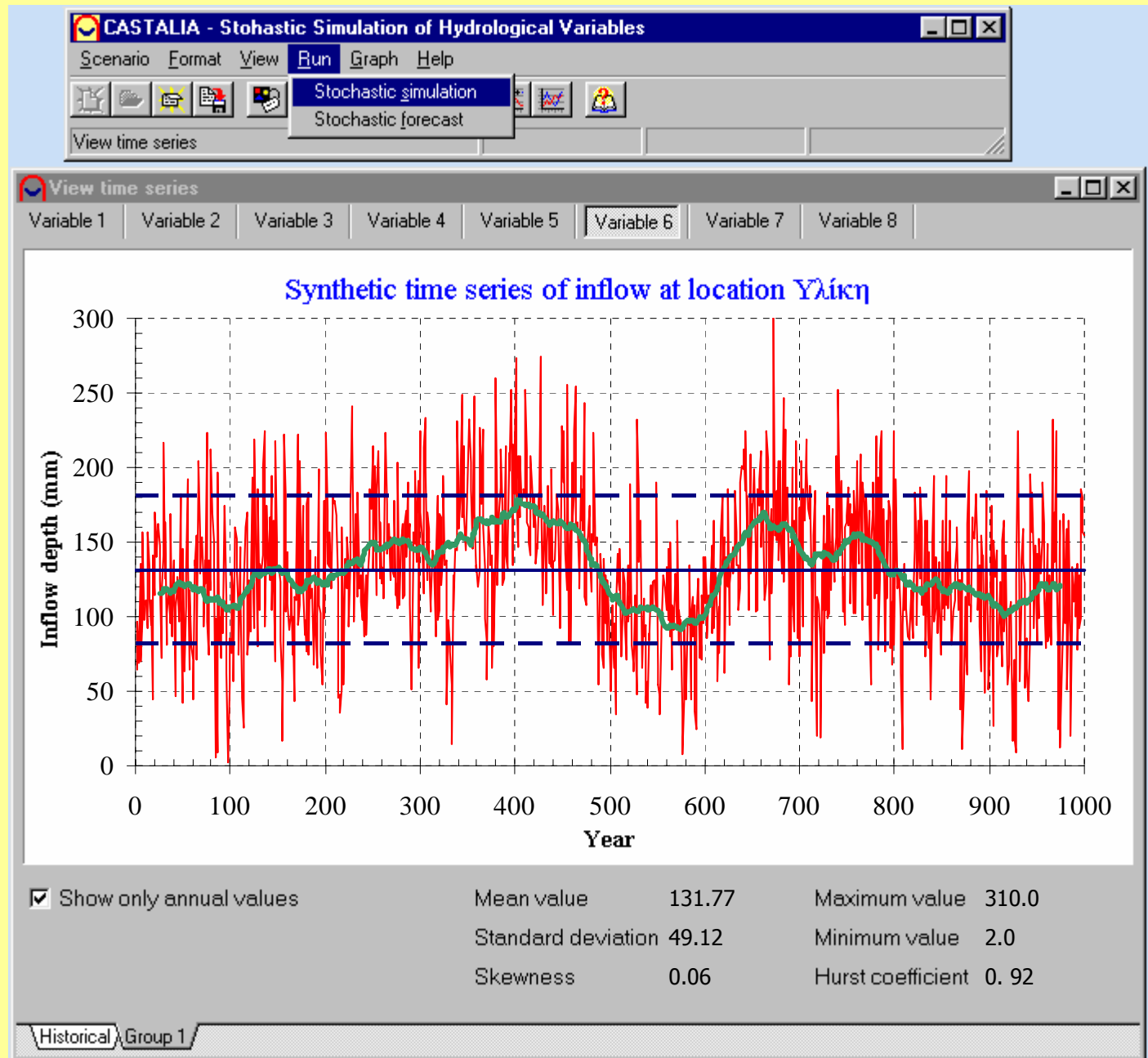
Castalia: Parameter estimation- Parameters of autocorrelation and persistence



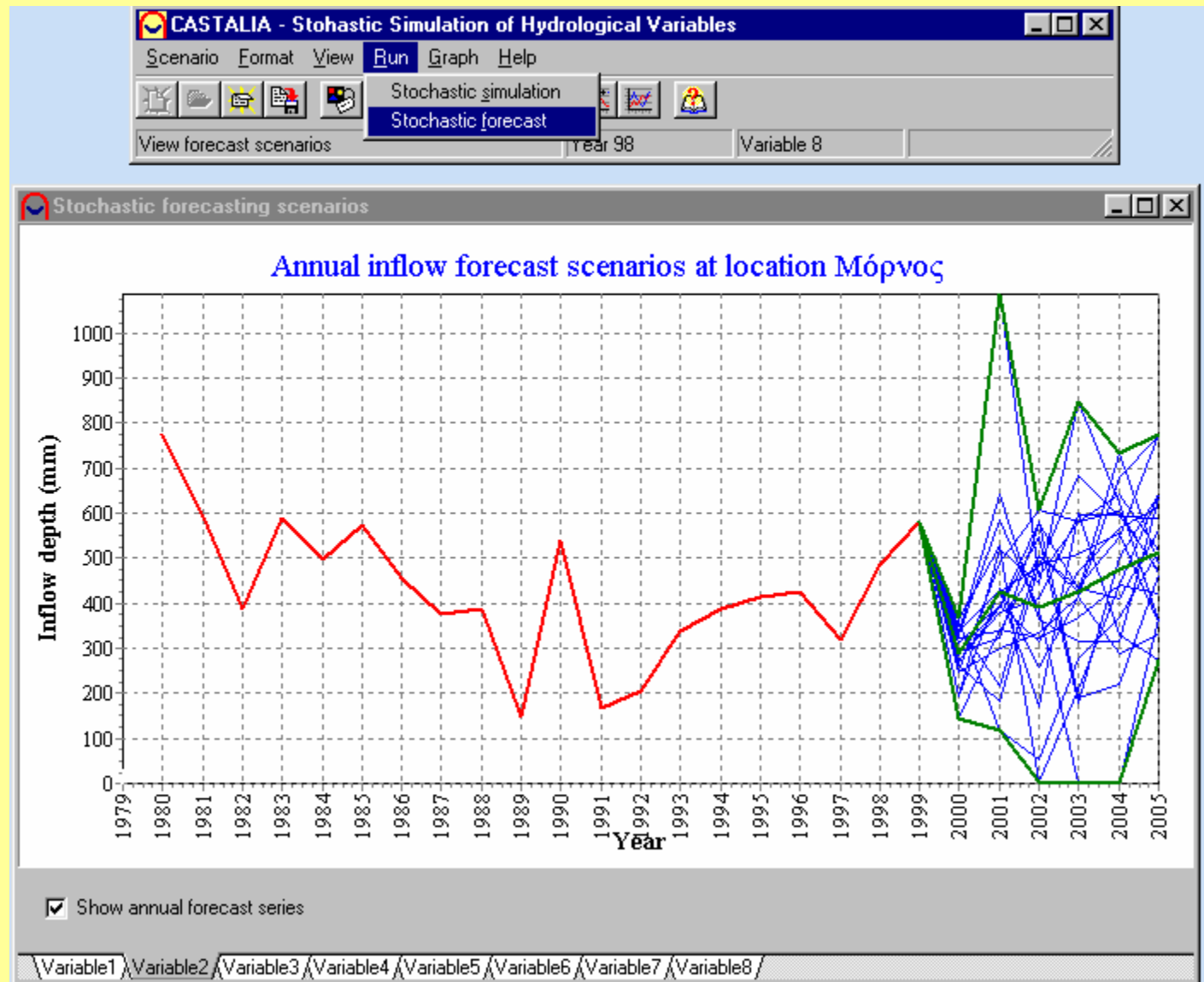
Castalia: Stochastic simulation without long term persistence



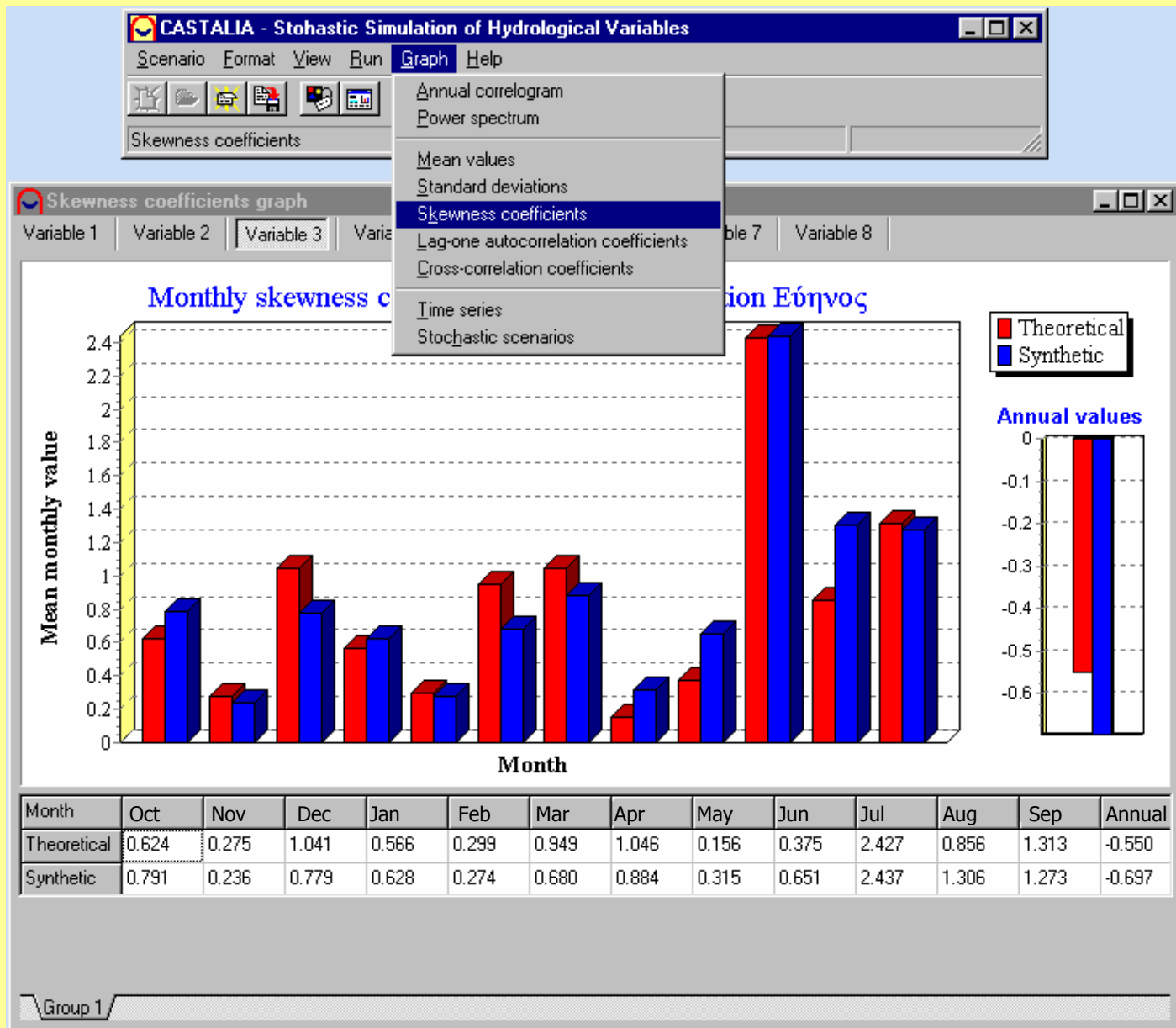
Castalia: Stochastic simulation with long term persistence



Castalia: Stochastic forecasting with long term persistence



Castalia: Preservation of marginal statistics – Skewness



Hydronomeas: Hydrosystem data management

Φόρμα Κόμβου/Ταμιευτήρα

Ο κόμβος είναι ενεργός

Όνομασία:

Είδος κόμβου

Απλός κόμβος

Ταμιευτήρας

Συντεταγμένες

Τετημένη:

Τετανυμένη:

Διαχείριση ταμιευτήρα

Διαχείριση ενεργή

0 Σταθερός όγκος

Νεκρός όγκος:

Χωρητικότητα:

Αρχικός όγκος:

Έκταση υπολεκάνης:

Φόρμα Προτεραιότητας Στόχων και Φόρμα Στόχοι

Συνιστώσα δικτύου	Κατανάλωση νερού - Ύδρευση (hm3)	NAI	53.300	1.000
1 Μουρίκι-Κρεμμάδα - 14/3/01	Κατανάλωση νερού - Ύδρευση (hm3)	NAI	23.600	1.000
2 Ζήτηση Μενιδίου	Μέγιστος όγκος (hm3)	NAI	600.000	1.000
3 Ζήτηση Γαλατσίου	Κατανάλωση νερού - Ύδρευση (hm3)	NAI	2.600	1.000
4 Ζήτηση Κιούρκων				
5 Ζήτηση Μάνδρας				
6 Μόρνος				
7 Εύηνος				

Προτεραιότητα Διαγραφή Στοιχεία

Φόρμα Υδραγωγείου

Το υδραγωγείο είναι ενεργό

Όνομασία:

Ανάντη κόμβος:

Κατάντη κόμβος:

Κατεύθυνση ροής

Μονοσήμαντη

Αμφίδρομη

Φόρμα Γεώτρησης

Η γεώτρηση είναι ενεργή

Όνομασία:

Κόμβος:

Κατανάλωση ενέργειας kWh/m³:

Άνω κατώφλι:

Κάτω κατώφλι:

Μέγιστη παροχή

Μηνιαία διακύμανση στόχου: Ζήτηση Γαλάτσι - 14/3/01

Μήνας	Τιμή στόχου
1	0.105
2	0.09
3	0.068
4	0.063
5	0.055
6	0.06
7	0.058
8	0.082
9	0.1
10	0.105
11	0.098
12	0.11

Φόρμα Ιδιοτήτων Στόχου

Γράφημα

Ο στόχος είναι ενεργός

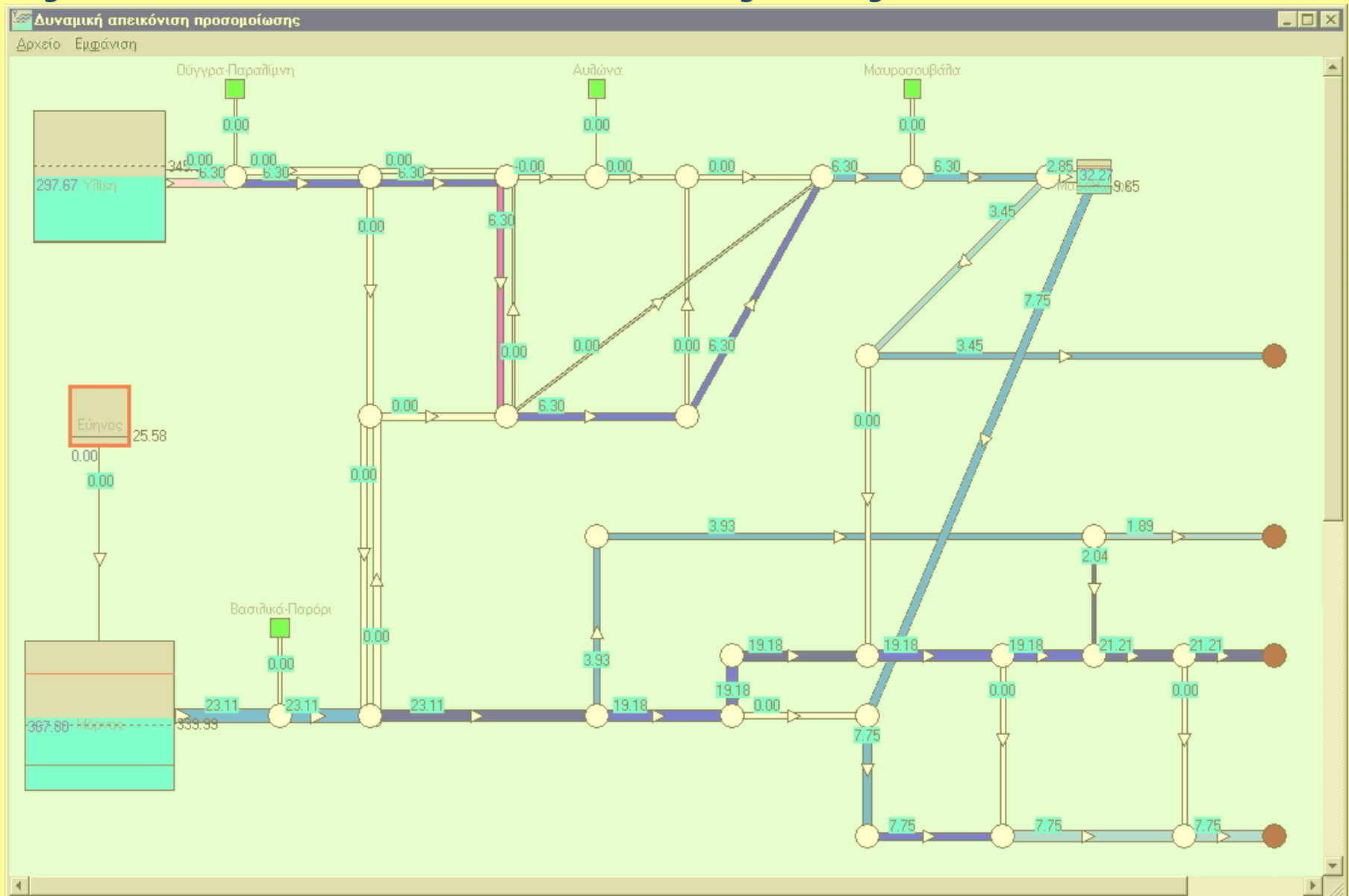
Όνομασία:

Είδος:

Αγωγός:

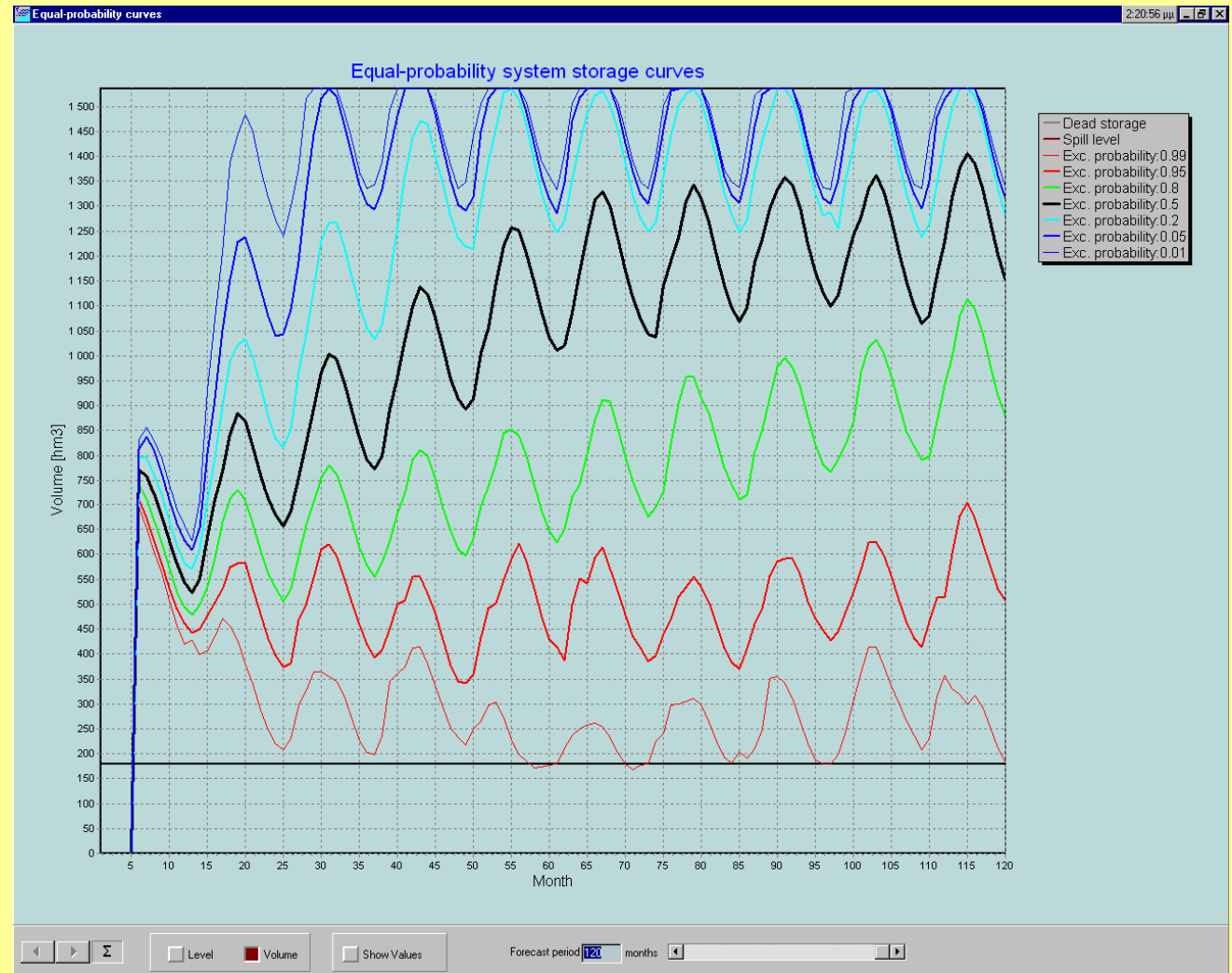
Μέγιστη αστοχία:

Hydronomeas: Visualization of hydrosystem simulation



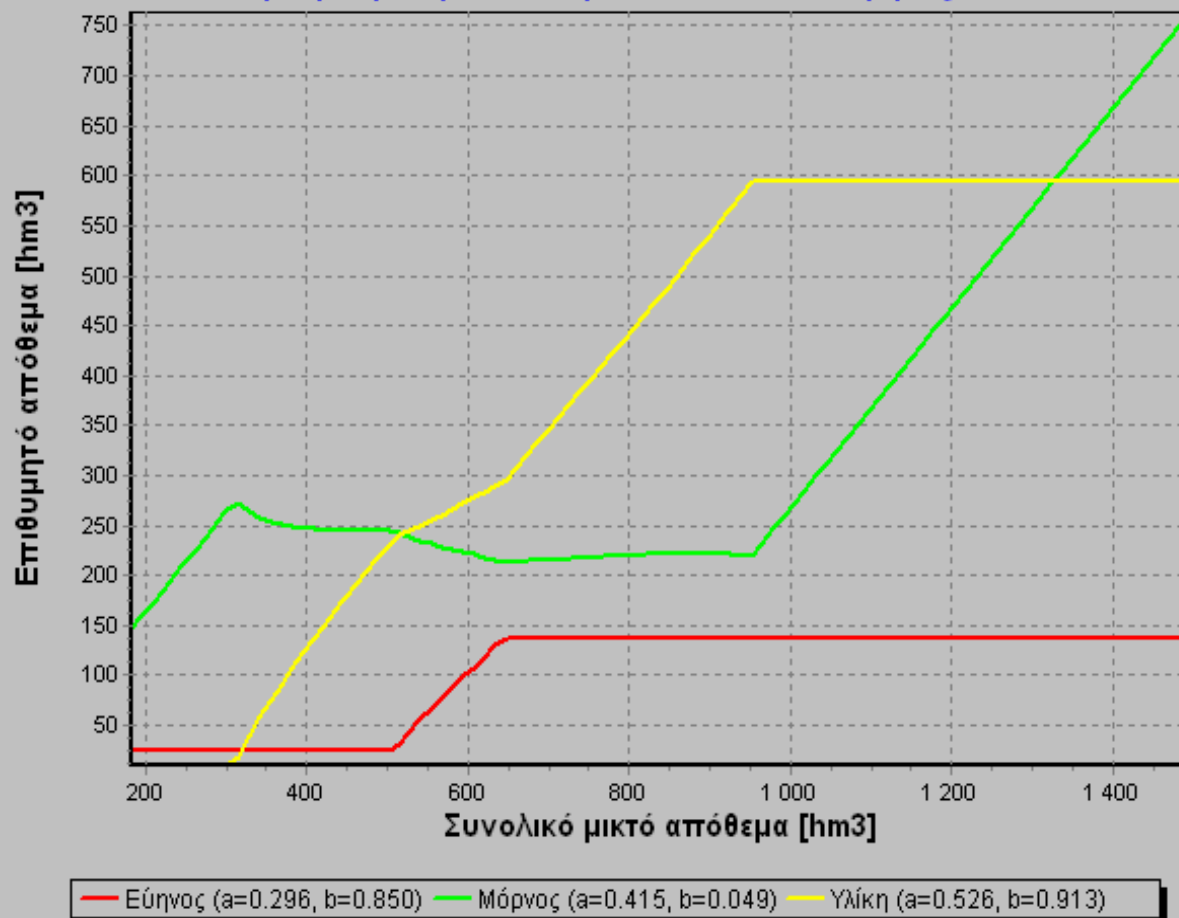
Hydroneas: Stochastic forecast of hydrosystem storage

Evolution of quantiles of system storage (for several levels of probability of exceedance) for the next 10 years as a result of 200 terminating simulations with long-term persistence



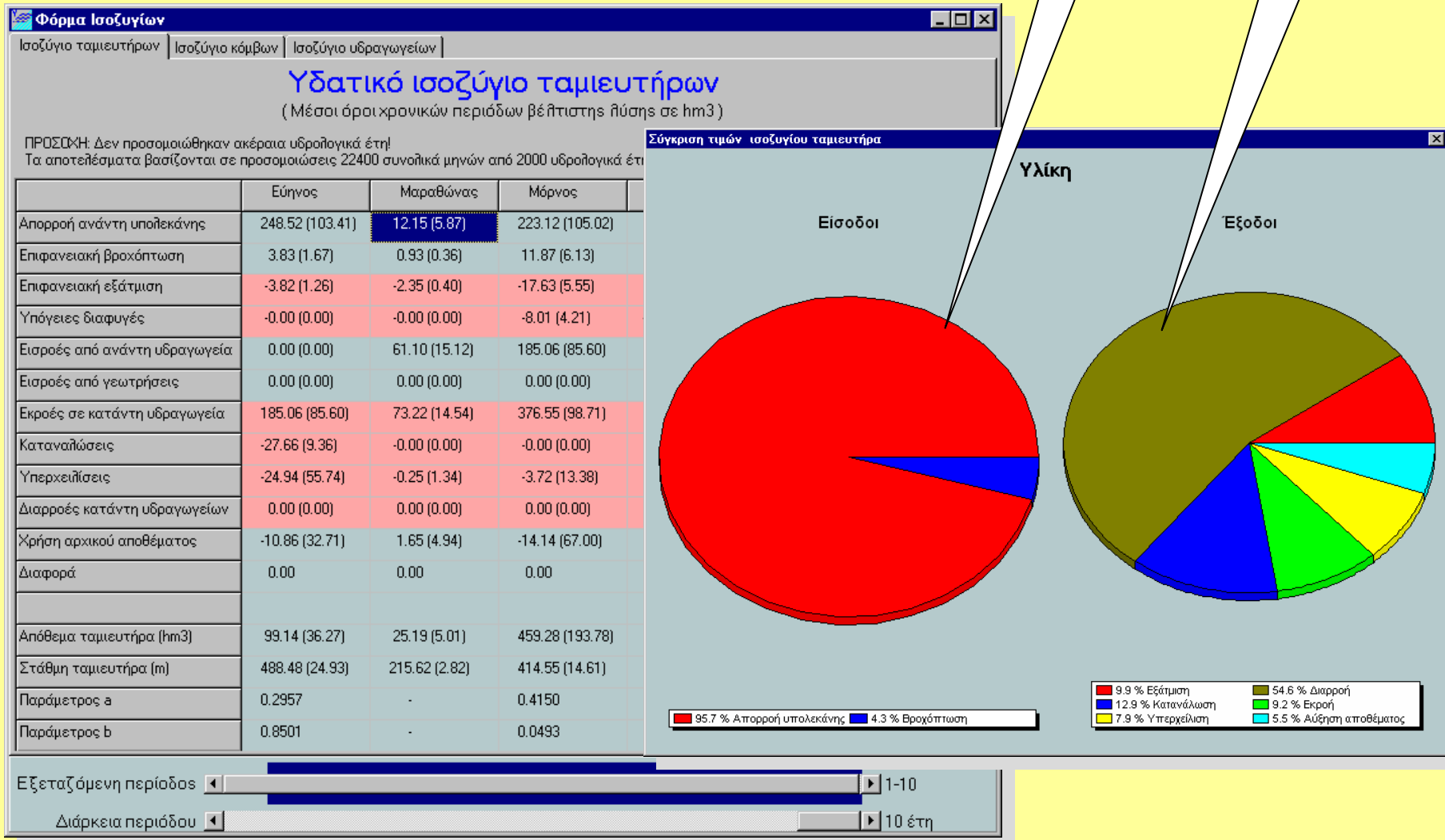
Hydronomeas: Optimal hydrosystem control rules

Γραφική παράσταση κανόνων λειτουργίας



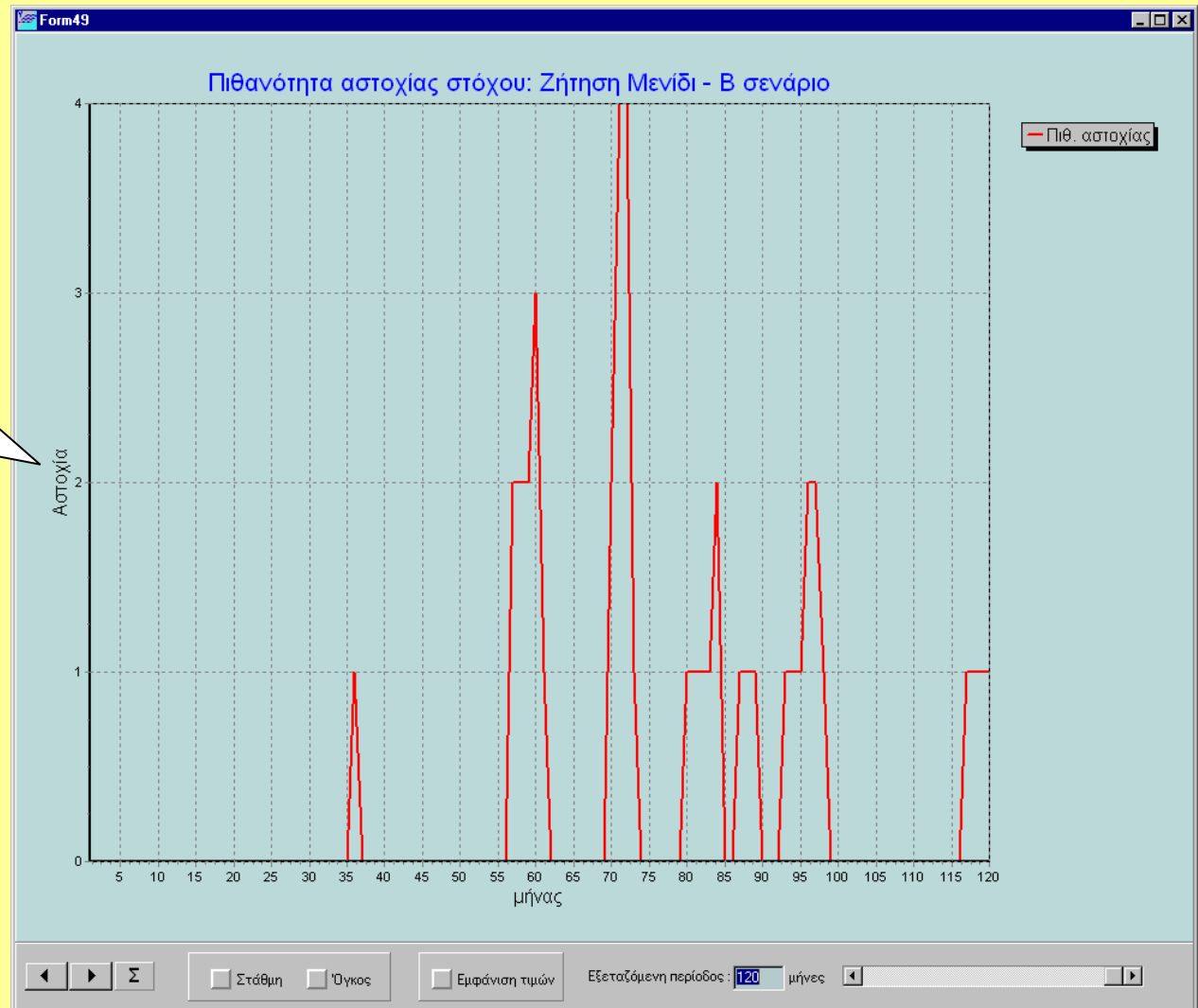
Target allocation of total reservoir storage per each reservoir

Hydronomeas: Reservoir balance



Hydronomeas: Time profile of failure probabilities

Number of failures in a total of 200 stochastic scenarios



Hydronomeas: Reporting

Print Preview

Υ
Υδρονόμος 2.1 - Εθνικό Μετσόβιο Πολυτεχνείο

ΑΣΤΟΧΙΑ ΕΝΕΡΓΩΝ ΣΤΟΧΩΝ (με σειρά προτεραιότητας)

Όνομασία στόχου	Περιγραφή	Αστοχία υδρολογικών περιόδων	Ανώτατη αποδεκτή αστοχία	Αστοχία μηνών	Αστοχία όγκου
Ελάχιστη ροή υδραγ. Υλίκης	Ελάχιστη ροή υδραγωγείου Υλίκης τους πρώτους μήνες προσαρμογής για υλοποίηση υποχρεωτικής απόληξης	0 / 2000	1.00	0 / 24000	0.00 / 0.00
Ζήτηση Μενίδι - 14/3/01	Επιθεώρηση σε ετήσια βάση και επεξεργασία κωμικών στόχων ζήτησης νερού για ύδρευση (Σύνολο Αθήνας 440 hnt)	17 / 2000	1.00	48 / 24000	0.17 / 224.27
Ζήτηση Γαλάτσι - 14/3/01	Επιθεώρηση σε ετήσια βάση και επεξεργασία κωμικών στόχων ζήτησης νερού για ύδρευση (Σύνολο Αθήνας 440 hnt)	23 / 2000	1.00	50 / 24000	0.23 / 124.36
Ζήτηση Κιόρκια - 14/3/01	Επιθεώρηση σε ετήσια βάση και επεξεργασία κωμικών στόχων ζήτησης νερού για ύδρευση (Σύνολο Αθήνας 440 hnt)	23 / 2000	1.00	56 / 24000	0.13 / 51.61
Ζήτηση Μάνδρα - 14/3/01	Επιθεώρηση σε ετήσια βάση και επεξεργασία κωμικών στόχων ζήτησης νερού για ύδρευση (Σύνολο Αθήνας 440 hnt)	25 / 2000	1.00	63 / 24000	0.07 / 22.77
Μέγιστος Όγκος Μόρνου Περροχή Ευήνου	Επιθεώρηση μέγιστος όγκος για αποφυγή υπερχειλίσεων	894 / 2000	1.00	7304 / 24000	0.00 / 0.00
	Επιθεώρηση τετραβελονική προαγωγή 2,6 hnt, εισάγεται ως κοινά λάσπη	999 / 2000	1.00	2918 / 24000	2.77 / 29.90
Μέγιστος όγκος Μαραθώνα	Επίσκεψη μέγιστου όγκου για αποφυγή υπερχειλίσεων	862 / 2000	1.00	4653 / 24000	0.00 / 0.00
Ελάχιστος όγκος Μαραθώνα	Επίσκεψη κωμικών στόχων ελάχιστου όγκου για τη διατήρηση οπθόμενων ασφαλείας	1415 / 2000	1.00	2820 / 24000	0.11 / 17.07
Άρδευση Κωσταΐδας	Ζήτηση νερού για άρδευση της Κωσταΐδας. Παρουσιάζει έντονη εποχική διακύμανση.	16 / 2000	1.00	46 / 24000	0.16 / 35.00

Μόνο οι ενεργοί στόχοι χρησιμοποιούνται κατά την προσαρμογή/εξέλιξη προαγωγή
Η πηγή αστοχίας υδρολογικής περιόδου (Έτος) ορίζεται από το λόγο των υδρολογικών περιόδων με αστοχία προς το σύνολο των προσαρμοσμένων υδρολογικών περιόδων.
Αστοχία που αναφέρεται ως προς τη υδρολογική περίοδο διαπιστώνεται κατά την αστοχία ενός τουλάχιστον χρονικού βήματος (μήνας) της περιόδου.
Η προτεινόμενη λύση τηρεί τον περιορισμό της ανώτατης αποδεκτής πιθανότητας αστοχίας για κάθε στόχο.

16/3/2001 5:31:54 μμ 33

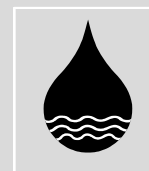
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Management plans and every day operation of the hydrosystem

- ◆ Every five years a master plan of the water supply of Athens is elaborated (the first was issued in 2000)
- ◆ Every year the master plan is revised based on current data and model runs
- ◆ Every three months the annual plan is reassessed and, if necessary, updated by new model runs
- ◆ Meanwhile, the every day management is based on optimal parametric operation rules
- ◆ Models are run for a 10-year lead time to account for long-term effects of today's decisions
- ◆ The general management targets are:
 - Adequacy of water resources
 - Adequacy of conveyance system
 - Cost effectiveness
- ◆ All management is based on a probabilistic approach of forecasts/risk/reliability assuming:
 - Acceptable reliability 99% on an annual basis
 - Potential for further increase of reliability taking into account elasticity of demand and emergency measures in case of impending failure
- ◆ So far, the decision support tool and its modules (thoroughly tested for the Olympics 2004) exhibited good performance

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Early stage



← The Hadrianean aqueduct

Supplementary water collection and distribution in Athens (early 20th century until 1930s)



Marathon dam



Construction of dam, 1928



Today

Construction of spillway, 1928



Marathon dam (2)



Devastating
flood, 1926



Inauguration of
Boyati tunnel, 1928



Marathon spillway
in action, 1941

Hylike lake and pumping stations



Hylike lake



Hylike, floating pumping stations



Hylike, main pumping station



Kiourka pumping station



Mornos reservoir and aqueduct



Mornos canal at Delphi



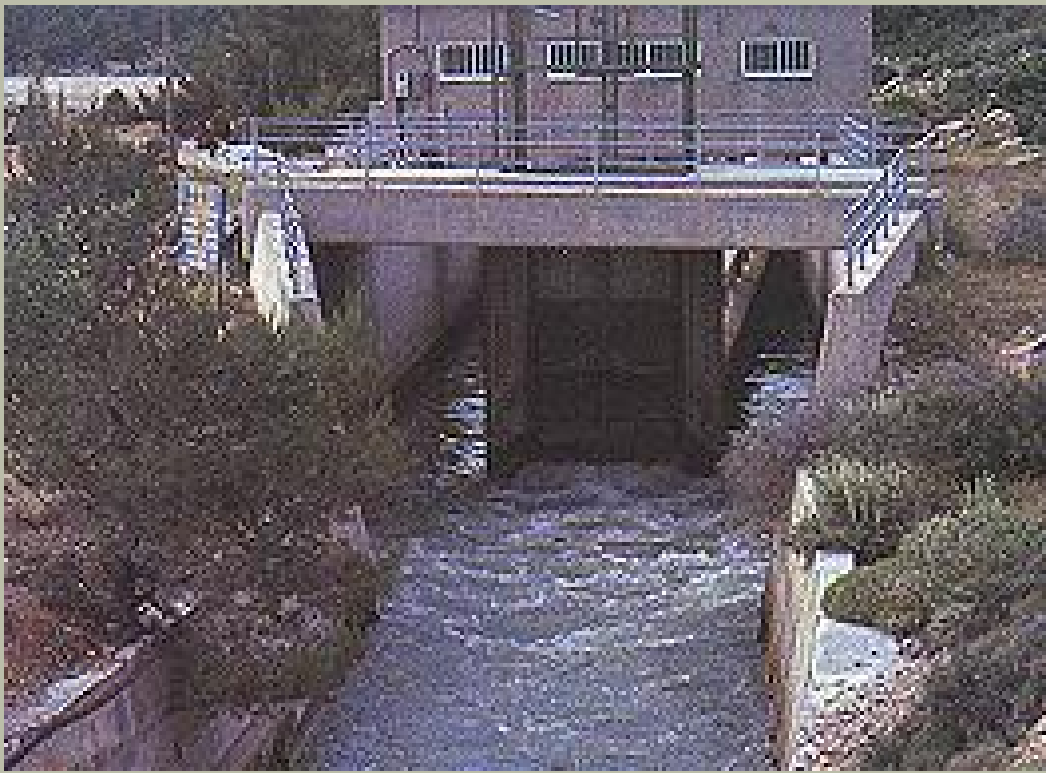
Mornos reservoir

Mornos canal at Thebes plain

Siphon at Distomo



Control of Mornos aqueduct



Canal flow control construction



Aqueduct supervizing & control centre



Evinos dam and tunnel



Evinos dam during construction

Construction of the Evinos-Mornos connection tunnel



Treatment plants



← Perissos water treatment plant



Aspropyrgos water treatment plant →